

9348

Bibl. Jo

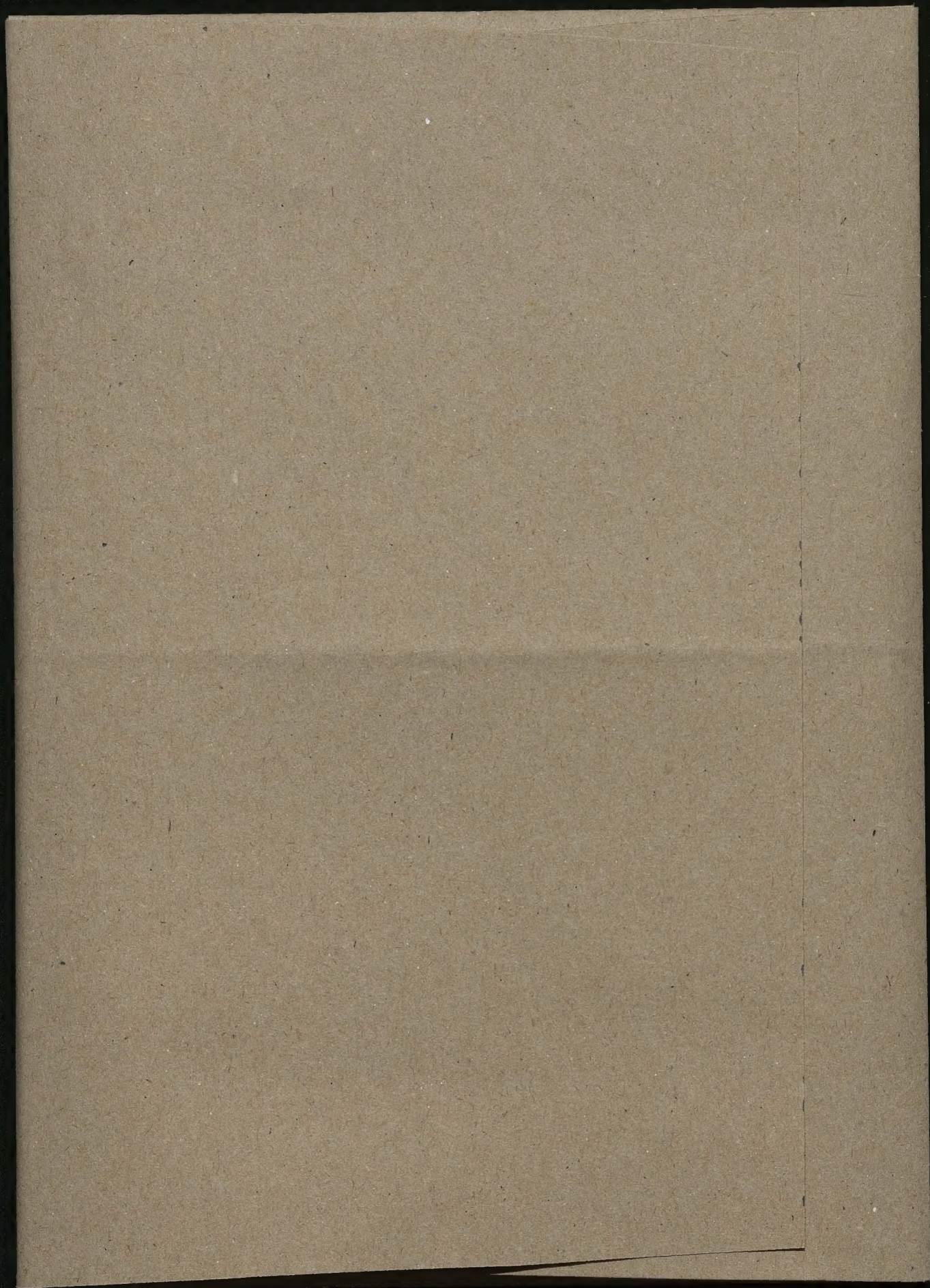
II

















mnijszych, <sup>i ze</sup> ~~Rozta~~ obliczenia Helmholtza, oparte na prawach dla cieplych idealnych, praktycznego zastosowania nie maja.

(Zastępnik ~~dotychczas~~ dotychczasowego zdanie i) <sup>podlega</sup> na  
 (Zastępnik) portowanie jest worych ~~zastępnik~~ <sup>wydotknięcia</sup> si ~~zastępnik~~  
 beśnadwini ~~cięż~~ <sup>wobec</sup> ~~zastępnik~~ <sup>wybrany</sup> ~~zastępnik~~ <sup>nie</sup> ~~zastępnik~~ <sup>zastępnik</sup>  
 zwykłym ~~zastępnik~~ <sup>zastępnik</sup> dla ~~cięż~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup> a ~~zastępnik~~ <sup>zastępnik</sup>  
 tegoż ~~zastępnik~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup>  
 występuje ~~zastępnik~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup>  
<sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup> ~~zastępnik~~ <sup>zastępnik</sup>







O portarami! iŝt' mery upphove's uph

ist u. in der ungenügenden

if every my system

the middle and  
near

inf. system v. den. sh.

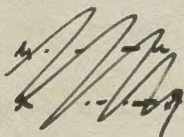






$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = \frac{\partial u}{\partial t} - \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right)$$

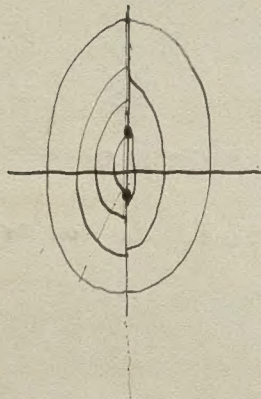
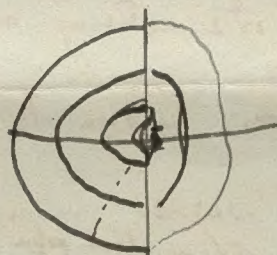
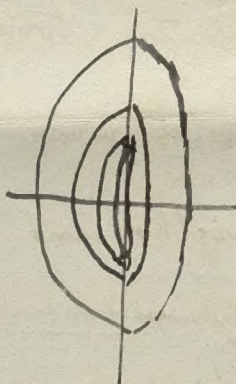
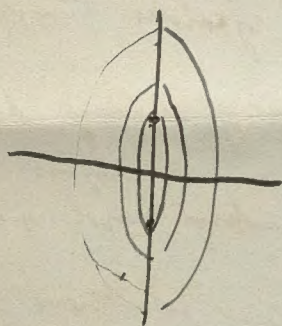
$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = \frac{\partial v}{\partial t} - \mu \frac{\partial^2 v}{\partial x^2}$$



$$\begin{array}{ll} u & \dots -u \\ v & \dots -v \\ w & \dots -w \\ \rho & \dots \rho - \rho \end{array}$$



$$\nabla \rho = \mu \nabla^2 v + (v \nabla) v$$



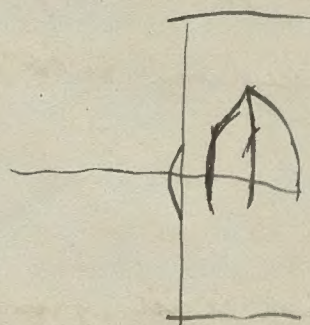
$$\mu \nabla^2 v = \nabla \rho - (v \nabla) v$$

$$\Delta \rho = 0$$

$$\rho = \nabla^2 v$$

$$\mu \nabla^2 v = \nabla \rho$$

$$= \nabla^2 u + \text{curl } \nabla^2 u$$

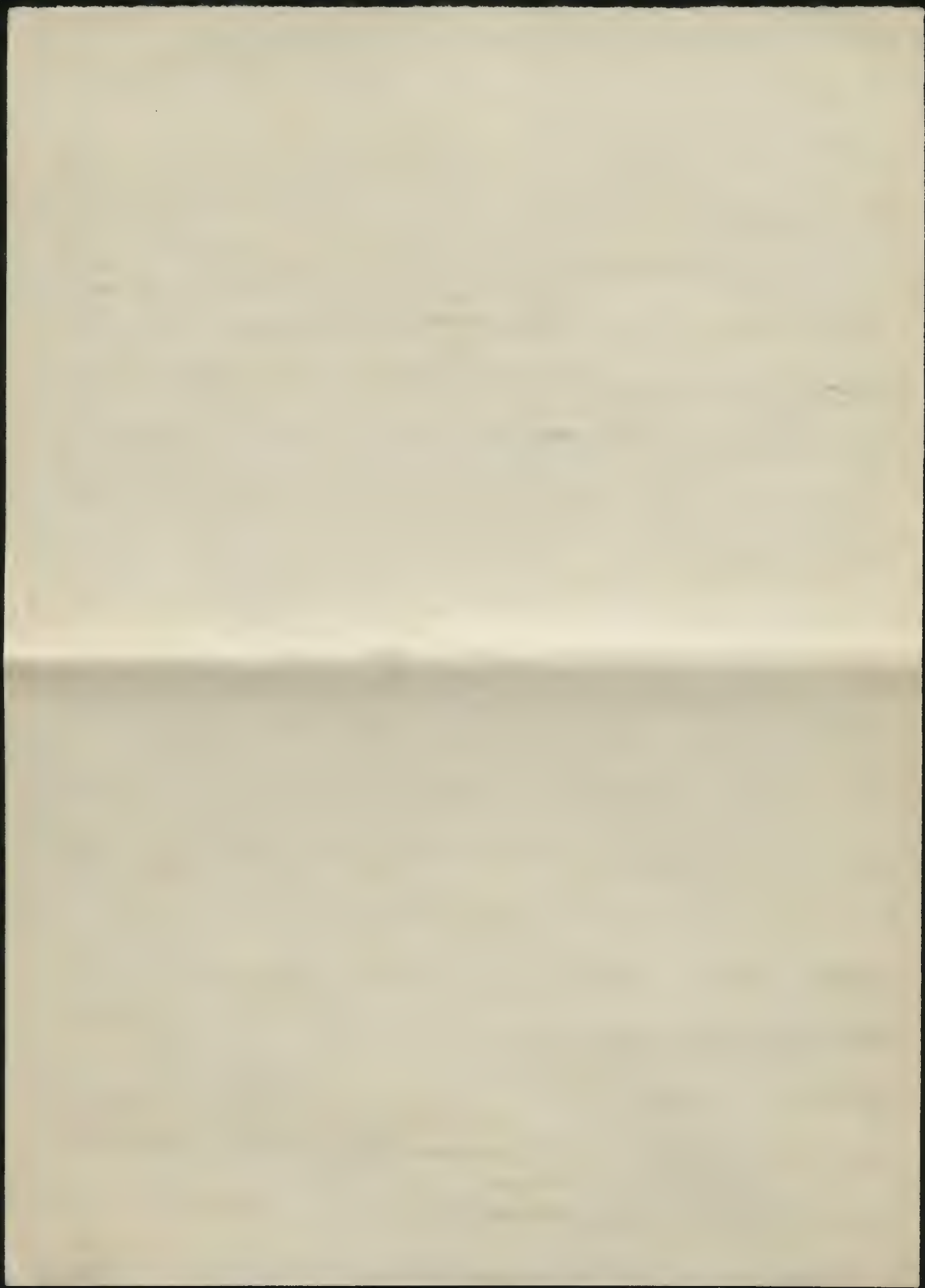


$$v = \nabla u + \text{curl } u$$





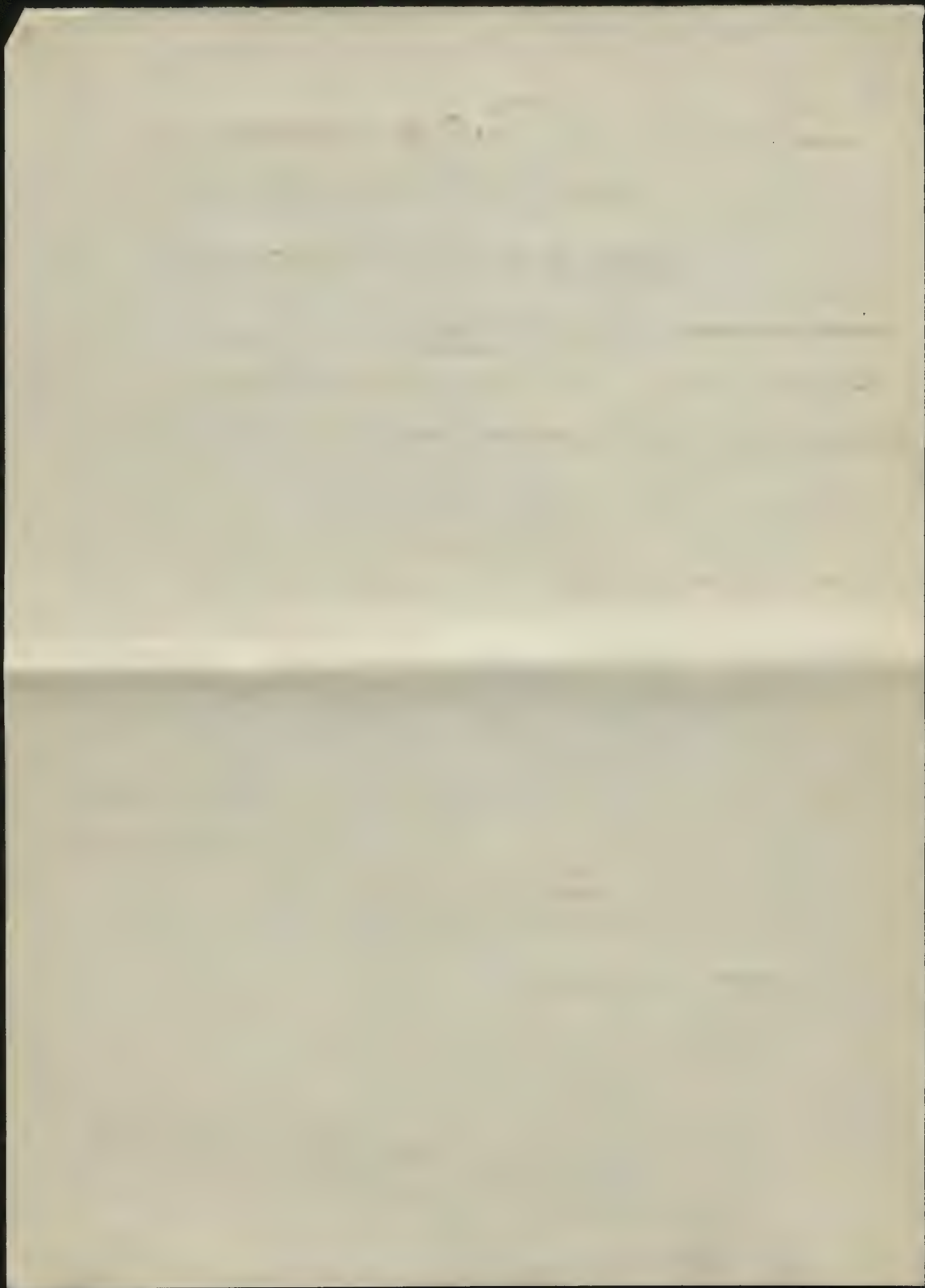








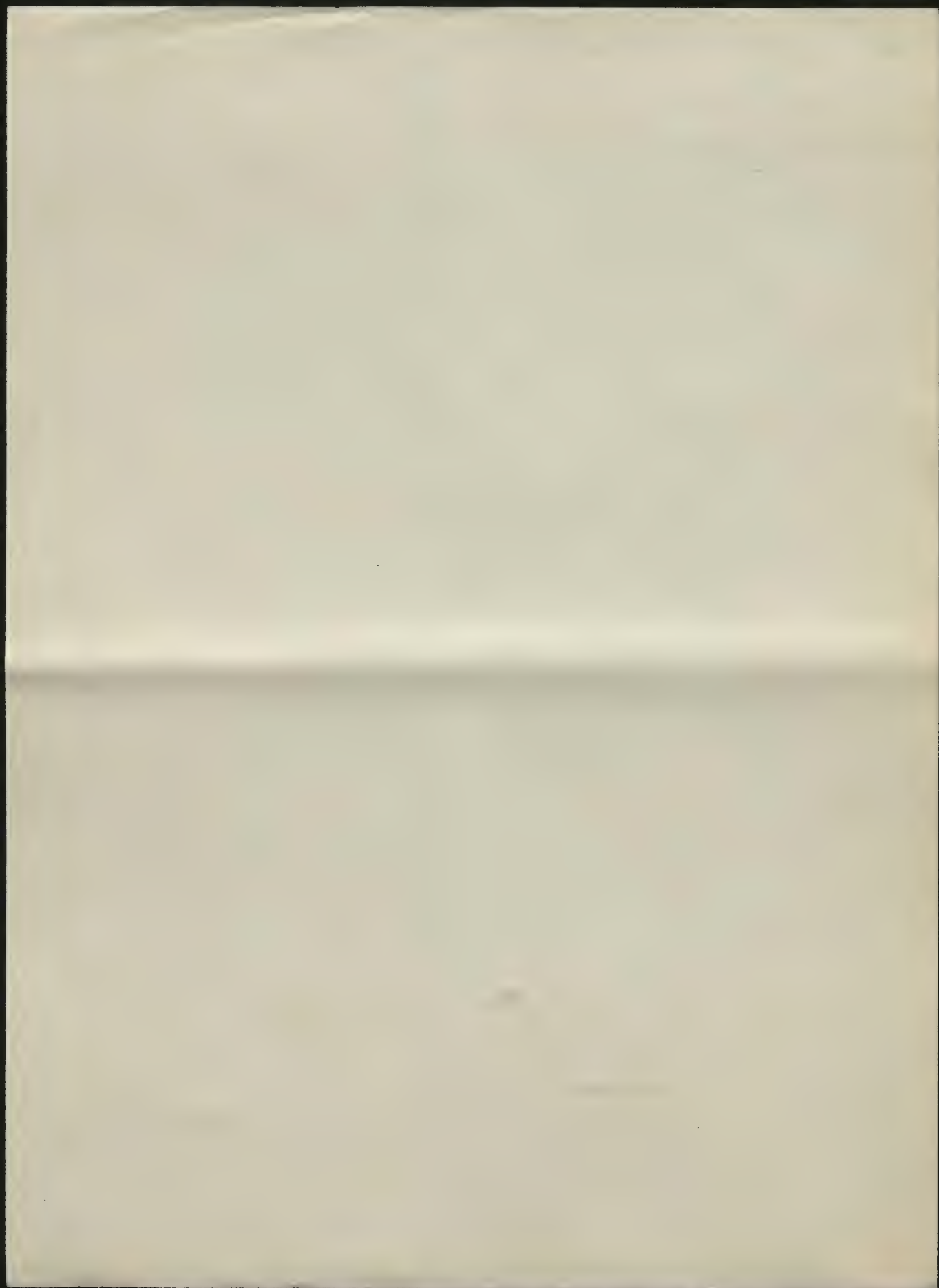








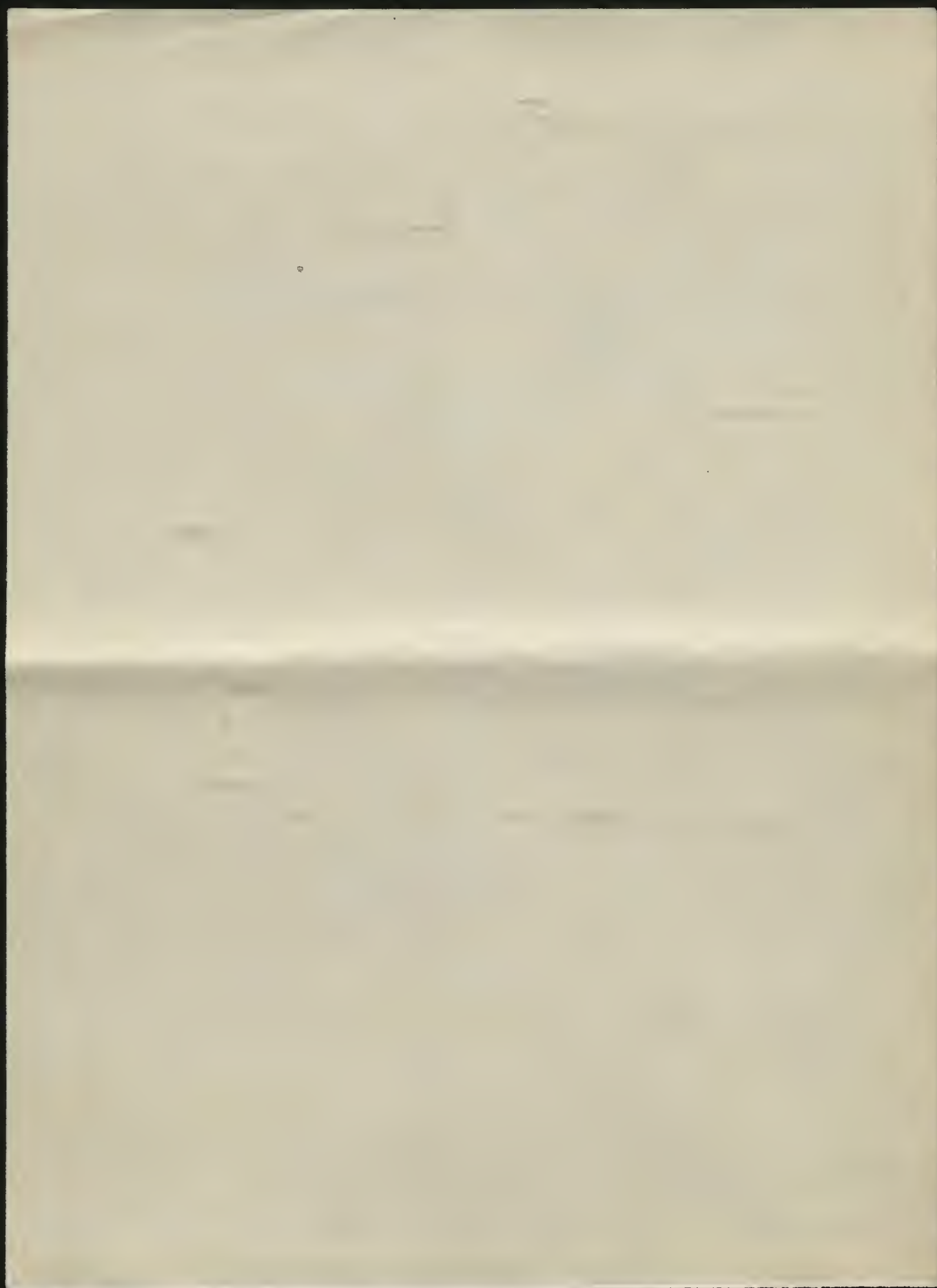


























$$\rho^{\frac{u}{x}} = t_x - \mu^{\frac{u}{x}}$$

$$\begin{aligned} \frac{\rho^u}{\mu} &= 1 & t &= \mu^u \\ & & &= \frac{\mu^2}{\rho} \mu \\ \mu &= \frac{\mu}{\rho} \mu_0 \end{aligned}$$



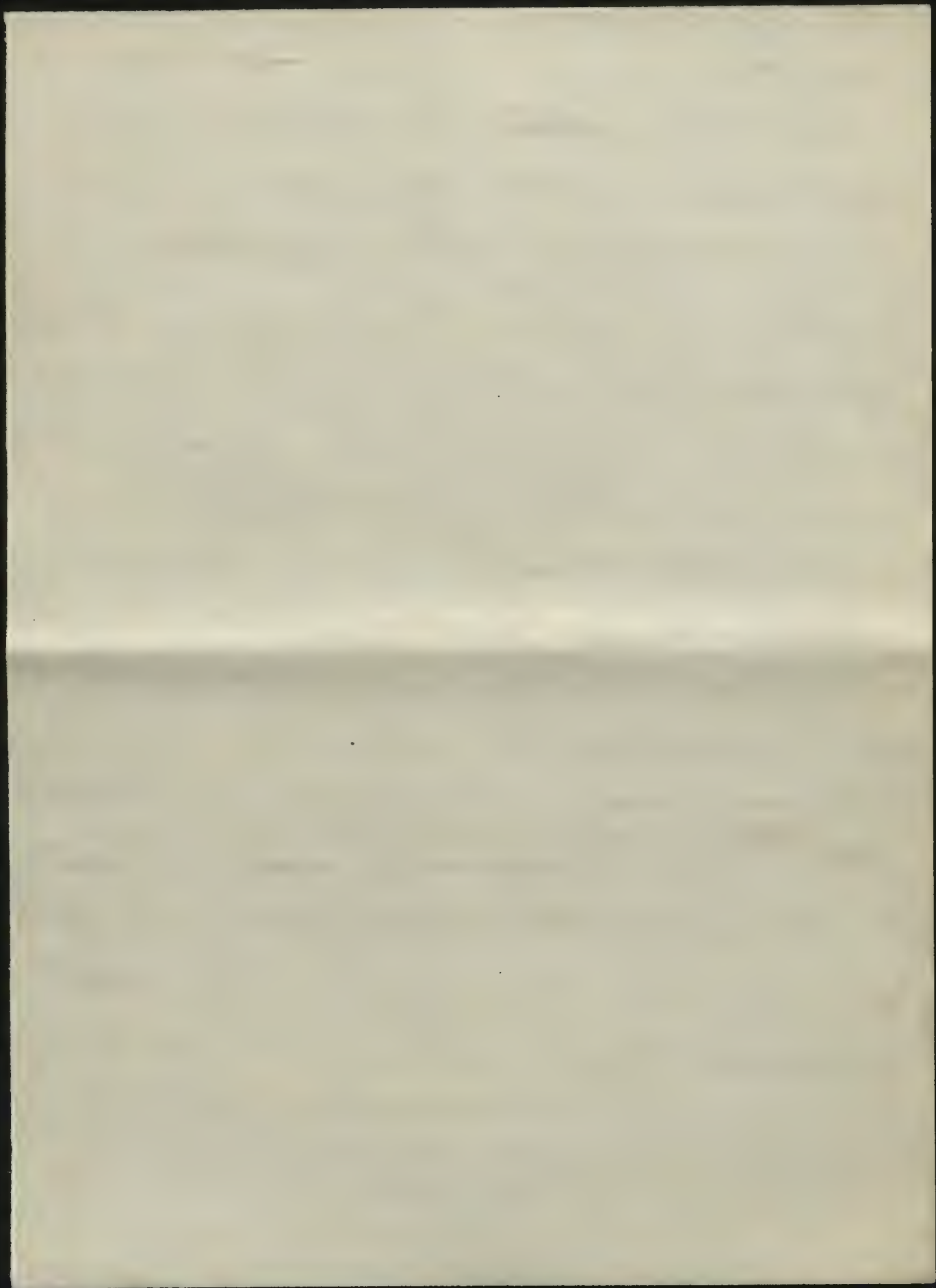
Nieby zbadać prawdziwości tego wniosku, przygotuję ~~naczynie~~ ~~do~~ ~~z~~ zbiornik<sup>9</sup>  
z którego ciecz wypłynęła, ~~jak~~ ~~to~~ naczynie do którego wstąpiła, jako też  
naczynie z którego wypłynął barwik rumianki wiodącemu do flaszki, z której  
poistnie mogłoby wypompuwać zapomocą pompy wodotryskowej.

[illegible][illegible]

$\Delta p_2 = \frac{\mu_2^2 p_1}{\mu_1^2 p_2} \Delta p_1$ , hydro to tedy much "dynamického podobnosti".  
 Jisli ztem nase tloucku efektivni prouku jst pravdivou, to  
 kratok linji prdu mui prouti nismimom, jisli uigrej uleg  
 muij nchleij ziskajmy prdku prdu u obrty stou u dlevoe,  
 i vpravo i vzhore

\* Nij nie powodem są - przede wszystkim niedostatek wiedzy i w szkole  
wydaje się ~~nie~~ bardzo poważnie z tym; można też użyć innych przykładów - ...









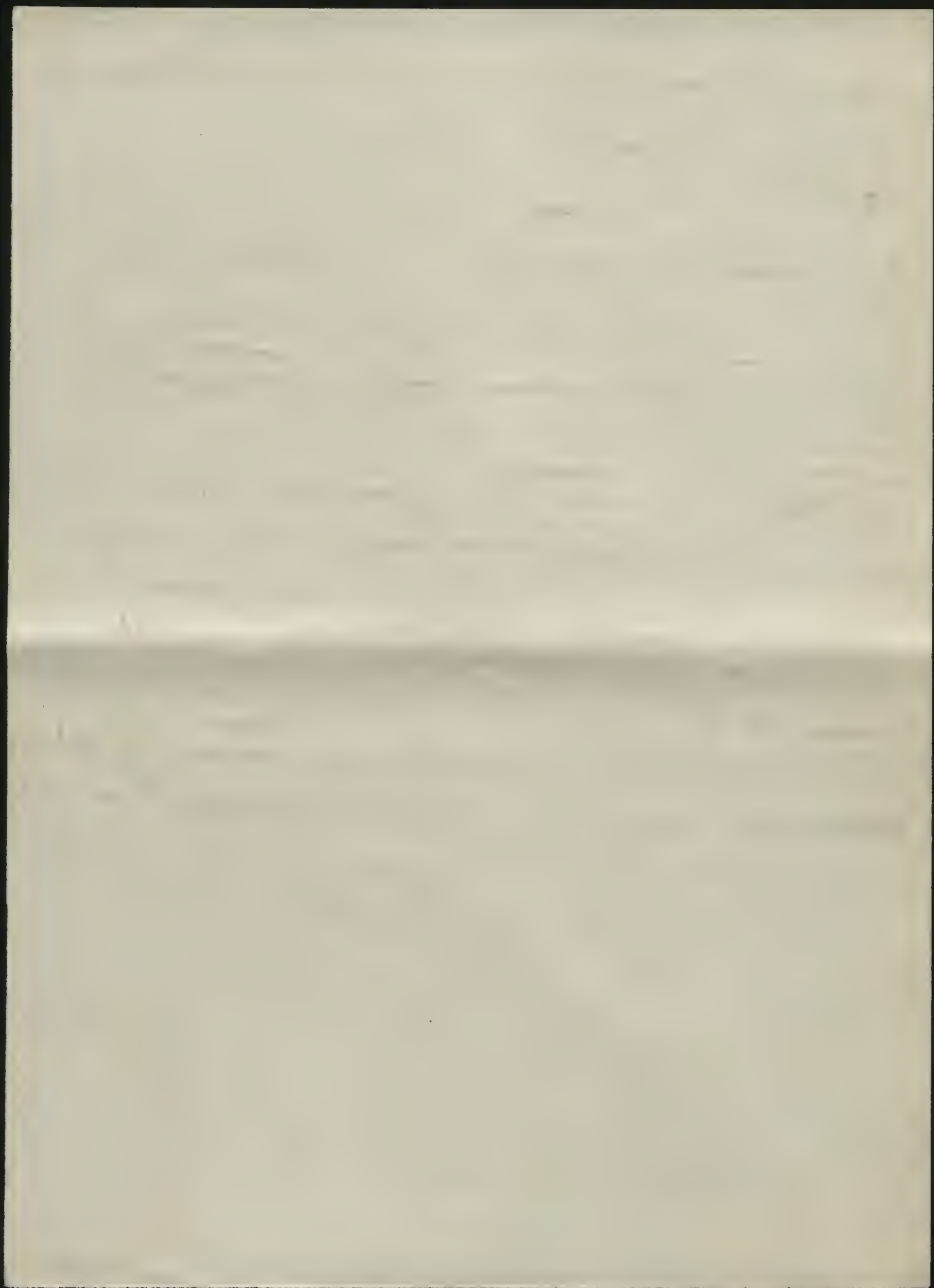








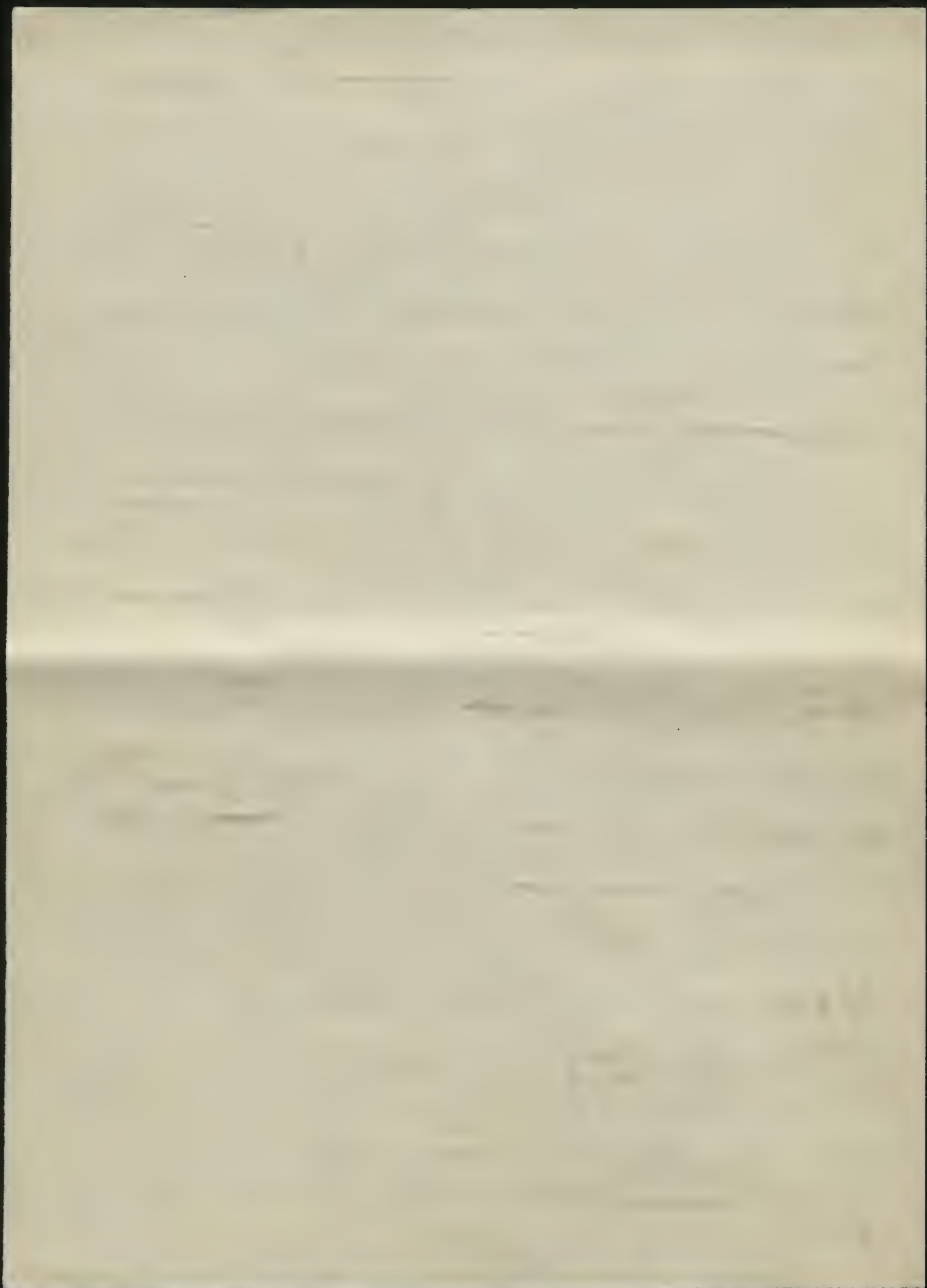














(13)

Fig... günzler kaiser

*Cory pernis per dromi*

obito in the afternoon  
~~in the afternoon~~

~~Adiantum~~ Adiantum

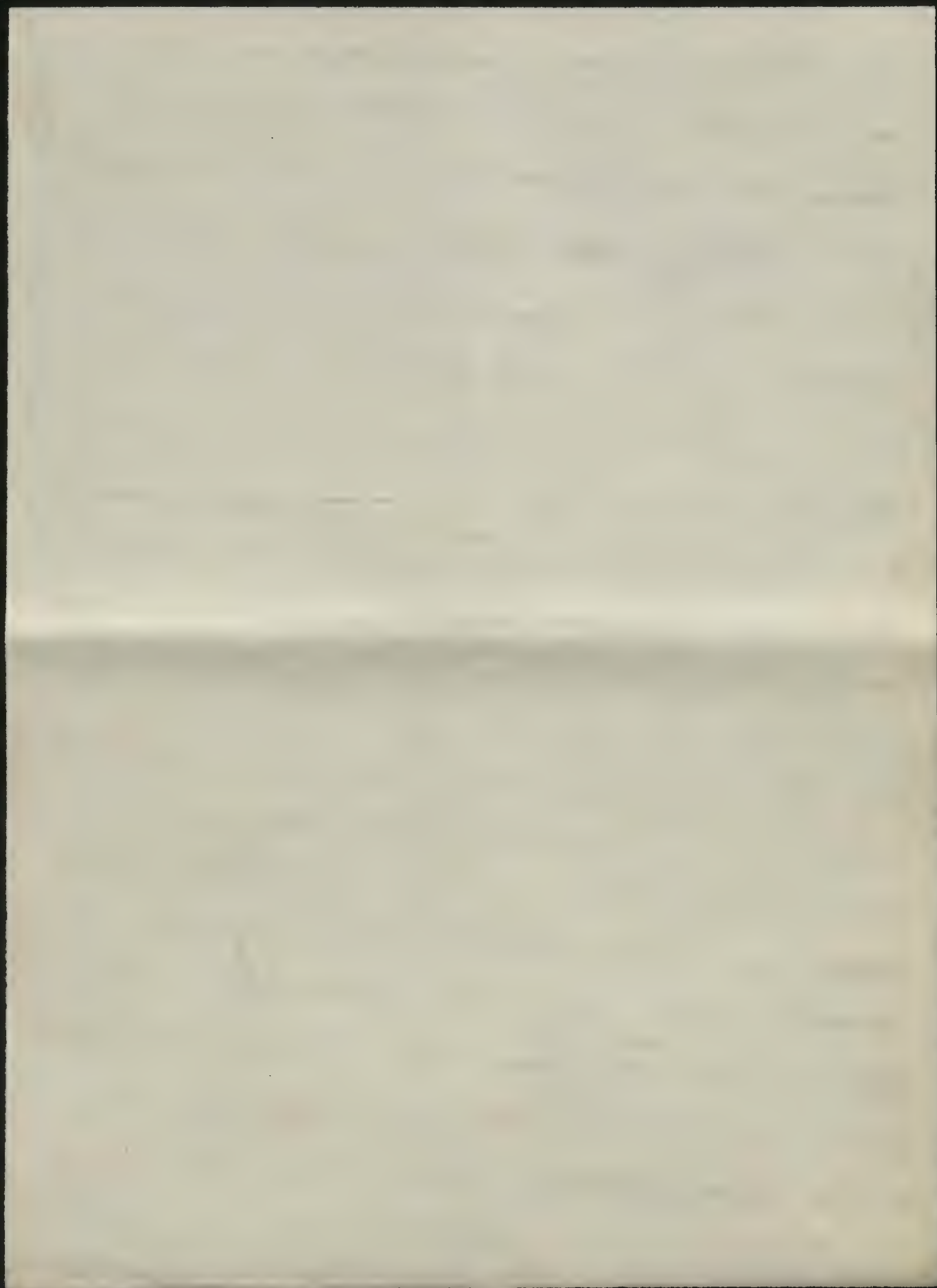
zjawiska

Pass.

moda by 1/2

~~24~~ 24  $\frac{m}{sec}$







(14)

we flange, & rotate tri

20th

od obnove potpis

~~W. Johnsoni~~ *peruviana*  
podrobný 2. výskyt v podstatě stejné

Wz. Równowagi emiendy w wygląd zaristki: ~~ten~~ ~~nie~~ przy ewolucji

any time

[illegible]

~~Masso~~ ariphanis pichlorus

*Wendlandia*

Tol.

Moimby przypuszczeń, że prędkość w. będzie „krzyżowa” tożs. z innymi

~~slavici~~ pydroni yzlyon

daru, mianorin a po p... ..

... ..

misleading by the 2 witnesses who charge

resin to the

*Vini de anni ~~1860~~ ni potlandis tipo pygmaeensis, ~~piceo~~*

[illegible][illegible][illegible]

Sacramentum purgationis huius propositi noster magister

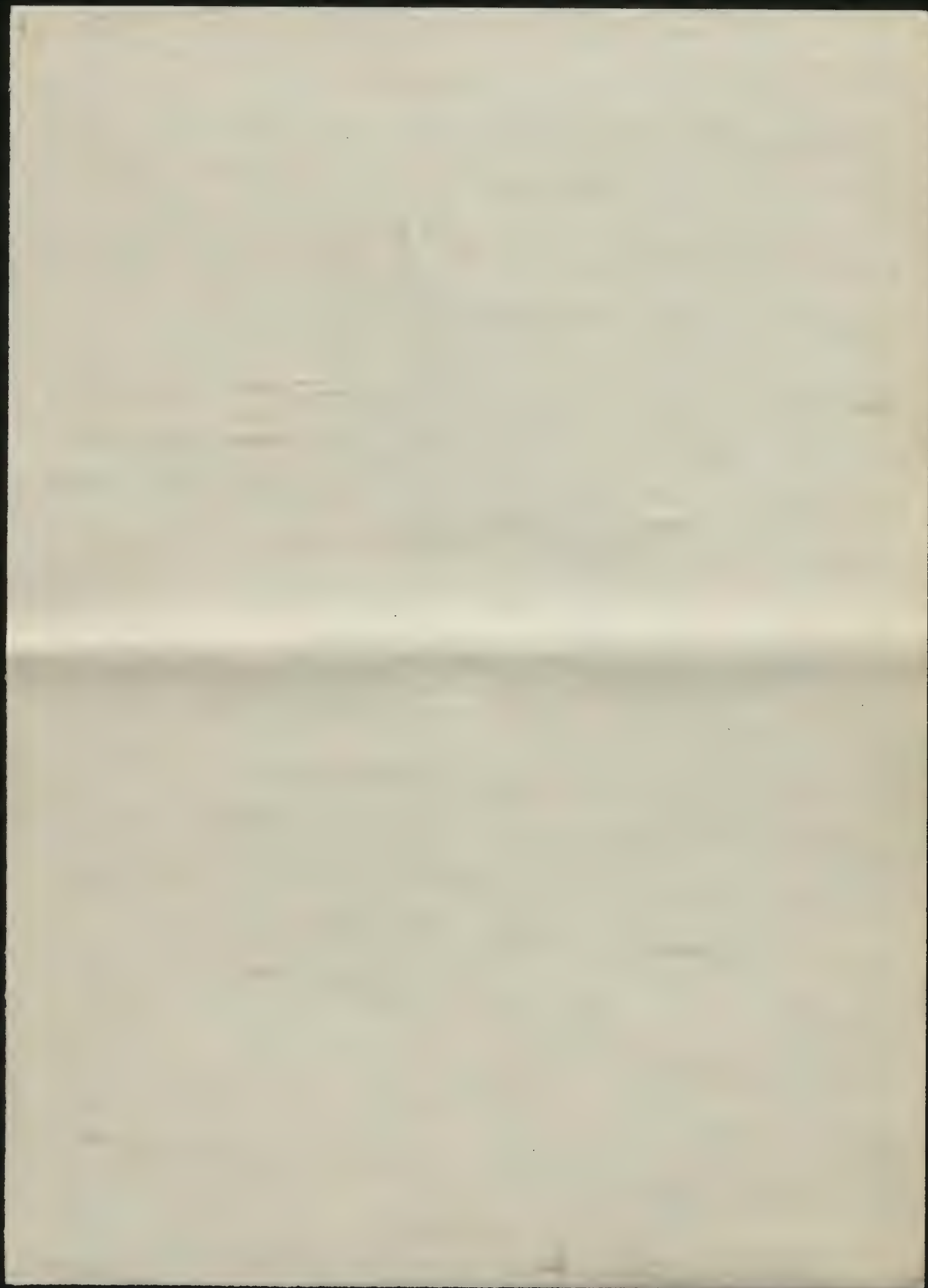
...kierunek sygnalizacji: lepkosć cieczy, która popiera

i endri onygh krypt onygh per...  
+ ... datukad idygh ididnygh i charaktirizatsii

*well known specimens of the same species.*

*Christenwege* ~~der Christen~~ der Christen







Ostotomne konkluzje z tytułu drinałdów są następujące  
Wyniki nasze mają straszyć i następują, a przede

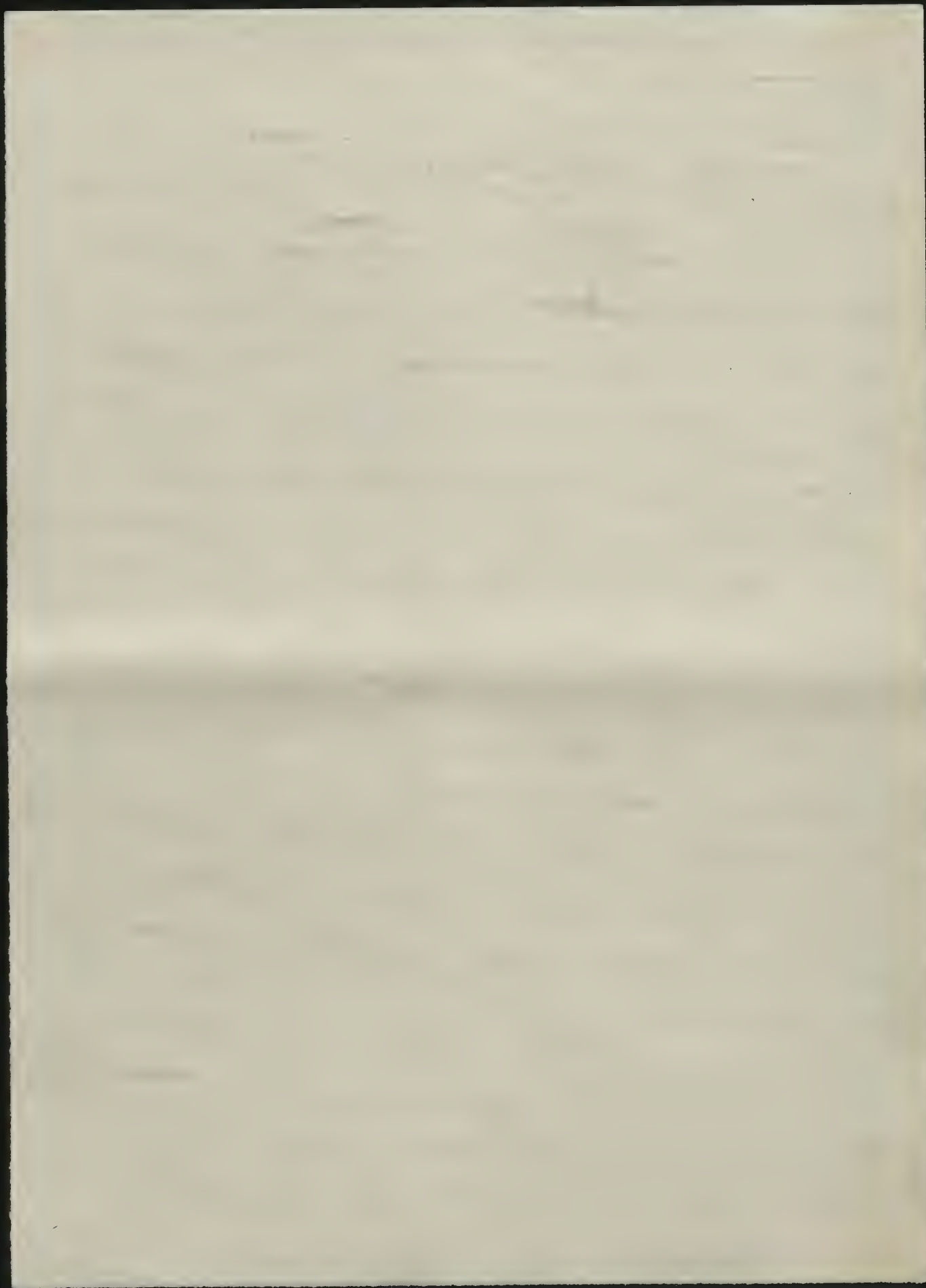
[illegible]

Co do postawienia "istoty wytycznej" drwina desenia wykazywały się ~~p~~<sup>o</sup> ~~z~~<sup>a</sup> tegoż  
dotyczy jest spільnymi przerwami w chwień dźwiękami smie podobnych dla ciężej kłopotach

Włocławek, 18.05.1944

Is just brown paper & indigo & redness & bluishness (turbid) & 2 postures of the  
in the mouth etc.



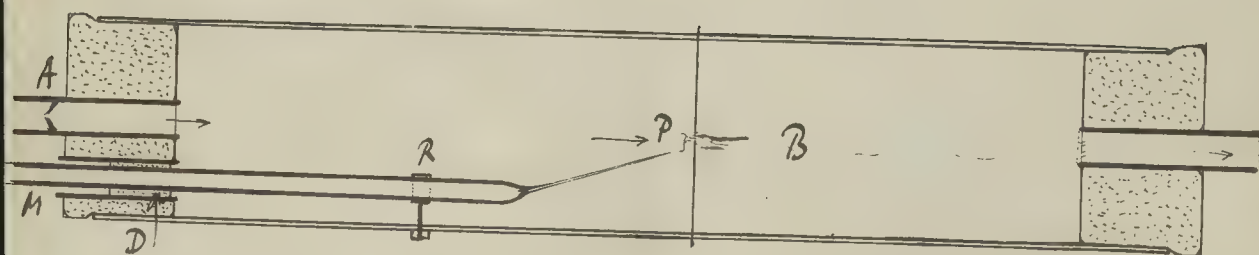












$$\frac{13.008}{60.00073} = \frac{13.4}{3.72} = 52 : 224 = \frac{26}{11} = 2.36$$

$$\frac{84.89}{74.7} = 83.9$$

$$2.36 : 74.7 =$$

$$\frac{18}{236.34} = \frac{18}{43}$$

$$\frac{54}{72} = \frac{3}{4}$$

$$\frac{6.12}{14} = \frac{0.0}{82}$$

$$\frac{18}{236.46} = \frac{18}{43}$$

$$\frac{1000}{2314} = 176$$

$$\frac{46}{368} = \frac{1}{8}$$

$$63432$$

$$\sqrt{3.4} = 1.85$$

$$\frac{18}{12} = \frac{3}{2}$$

$$\frac{185.14}{26} = 7.12$$

$$\begin{array}{r} 424/4 \\ 1449 \end{array}$$

$$\begin{array}{r} 162 \\ 136 \\ \hline 256 \\ 136 = 225 \end{array}$$

$$\sqrt{2.4} = 1.40:2$$

$$\begin{array}{r} 1.55 \\ 6.2 \\ \hline 2.17 \end{array}$$

$$.44$$

$$\sqrt{7.35}$$

$$= 1.10.14$$

$$\begin{array}{r} 78.2 \end{array}$$

$$\sqrt{0.66}$$

$$= 0.8.14$$

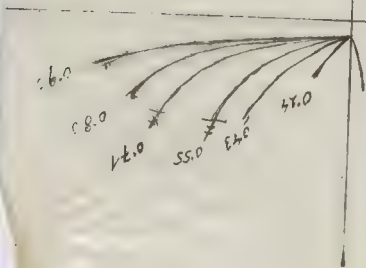
$$\begin{array}{r} 14.2 \end{array}$$

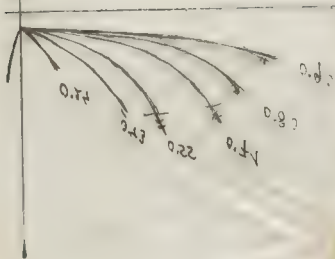
$$\rho \frac{u^2}{x} = \frac{k}{x} = u \frac{u}{x}$$

$$\rho u^2 = k = u \frac{u}{x}$$

$$\rho u^2 = \frac{d}{dx} u$$

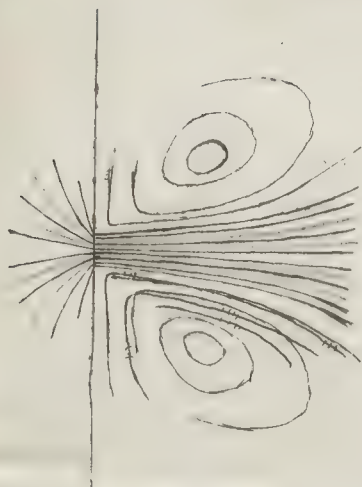




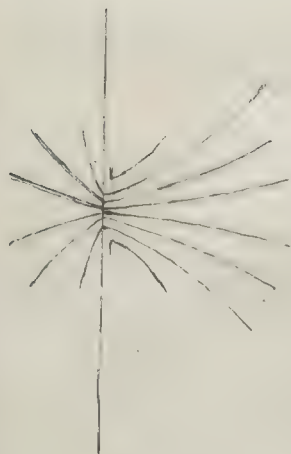




(0'8,5)

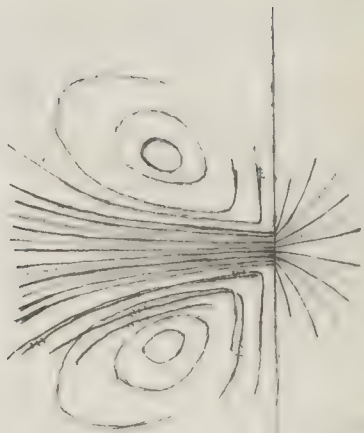


0'450



27

(0.80)



(0.2)





(0° 230 ')



0° 170



0° 232



0° 170

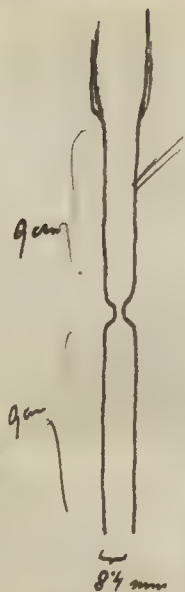




$$\begin{array}{lcl}
 183 \text{ Kugle. Slyn. II} & = & 180 \\
 180 & & 179 \\
 143 \text{ natv. } 21'30'' & & = 144 \text{ white} \\
 133 \text{ vnd. up to } 190 & & \equiv
 \end{array}$$

$$\begin{array}{r}
 8230 \\
 1416 \\
 \hline
 2314 \\
 \text{Horse}
 \end{array}$$

$$\begin{array}{r}
 5010 \\
 4935 \\
 \hline
 1155 \text{ g.}
 \end{array}$$

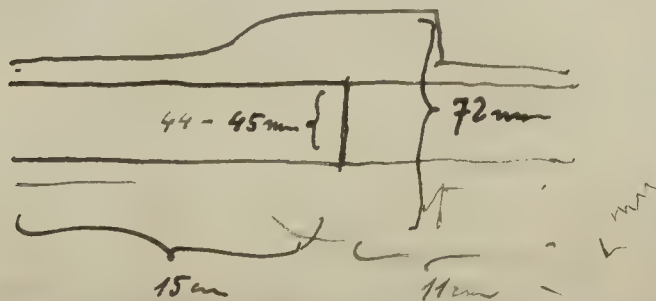
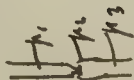


$$\begin{array}{lcl}
 0.93 & \} & \text{putting together} \\
 1.00 & &
 \end{array}$$

$$\begin{array}{lcl}
 0.095 \text{ mm} & \text{thick} & \text{measuring} \\
 2.4 & \text{thin} & \text{line}
 \end{array}$$

$$p_{02}^2 =$$

$$p_{02}^2 = p_1 - p_2$$



$$2' 10.5'' = 130.5''$$

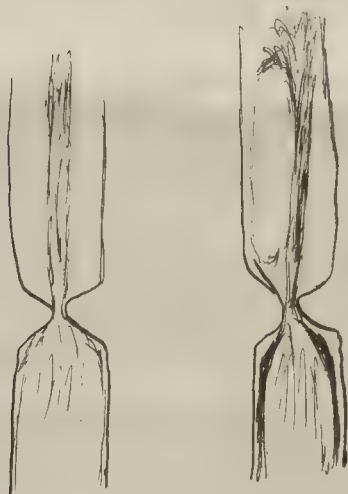
$$\left. \begin{array}{l} 2' 10 \\ 2' 5 \\ 2' 15 \\ 2' 12' \\ 2' 15 \end{array} \right\} 2' 11.4'' \quad \left. \begin{array}{l} 3' 52 \\ 3' 35 \\ 3' 45 \\ 3' 55 \end{array} \right\} 3' 47''$$

$$\left. \begin{array}{l} 4' 30'' \\ 15 \\ 20 \\ .75 \end{array} \right\} 4' 25''$$

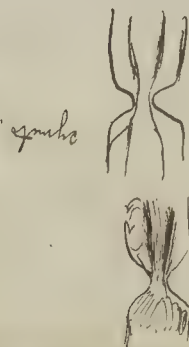
$$3' 187:4 =$$

$$57:5 = 11.4$$

$$= 47$$



(average)  
92



gambu

81

30 = 6

atm 2' 10"

3' 52"

2' 5"

4' 30"

2' 15"

4' 15" + (to middle pr)

4' 30"

3' 35"

3' 45"

2' 12"

margin. gran. c

$$\begin{array}{r} 74.2 \text{ cm} \\ + 38 \end{array}$$

$$\begin{array}{r} 31.7 \\ 18 \end{array}$$

$$\begin{array}{r} 21.7 \\ + 38 \end{array}$$

$$\begin{array}{r} 21.7 \\ + 38 \end{array}$$

"

3.7

"

(68)  
Pny 24 cm size syringe 2 positive  
+ 38

tj. 2=0 dla P = 78 cm, p = 278



$$11'55 : 180 = 0'0$$

$$3'85 : 60 = 0'0642 \quad q^3 = 1 \text{ kupa Slyn II}$$

06258

25285

80973

06258

15836

90422

$$0'0645 \text{ cm}^3 = 1 \text{ kupa Slyn I}$$

$$0'0802 \text{ cm}^3 = \text{ " wsta. v.}$$

~~245. 3.14~~

0'245

0'1225

~~0'38917~~

0'08814 -1

0'17628 -2

0'49715

0'67343 -2

~~0'047786~~

$$0'047144 = \text{przekrój}$$

0'0802

0'0471

=

80917

0'67343

0'23074

$$= 1'70 \text{ cm}$$

$$\frac{1 \text{ kupa wsta.}}{\text{min.}} = \frac{1'70}{60} \frac{\text{cm}}{\text{sec.}} = 0'0283 \frac{\text{cm}}{\text{sec.}} \quad \text{przebieganie przedkroju w przekroju}$$

$$\frac{1 \text{ kupa II}}{1'37 \text{ u}} = 1'37 \text{ u}$$

$$0'093. 0'1. \pi = \frac{3'14}{992}$$

2826

$$\frac{0'0292}{4} \text{ cm}^2 = 0'0073 \text{ cm}^2 = \text{przekrój}$$

flanka na minutę :

2314

0'0073.60

=

2314

0'438

56436

04147

72289

36436

86332

50104

$$= 5283 \frac{\text{cm}}{\text{sec.}} = 52'83 \frac{\text{m}}{\text{sec.}}$$

Granica rozrywania

przy rozrywaniu w kierunku p

v

teoret. pkt. do wyłamania

41

25'5

cm

flanka

50104

42325

07779

11'96

m

8'24

14

10

27'8

cm

265"

50104

35603

14501

11'96

9'73

19

18

35'5

cm

227"

50104

11860

38244

24'12

14'42

26'3

P=3'4

78'0

cm

131'4"

22'05

$$\begin{aligned} \text{Gystron } \frac{\text{inter.}}{\text{wave}} &= \frac{1095}{1750} = 1.00085 = 1.0952 \text{ etc.} = 5.78\% \\ \frac{\text{Gystr. I}}{\text{wave}} &|_{20} = 1.095 = 1.094 \text{ etc.} = 37.5\% \\ \frac{\text{Gystr. II}}{\text{wave}} &|_{20} = 1.1166 = 45.8\% \end{aligned}$$

$$\mu_1 |_{\theta=17^\circ} = 0.01094$$

$$\mu_2 |_{\theta=19.7^\circ} = 0.03465$$

$$\mu_3 |_{1950} = \frac{1066}{114} : \frac{238}{19} = 4.48 \cdot 1.117 \cdot 0.01024$$

$$= 0.05124$$

$$\begin{array}{r} 3.384 \cdot 1024 \\ 08 \\ 14 \\ \hline 3466 \end{array}$$

$$\begin{array}{r} 65128 \\ 04805 \\ 01030 \\ \hline 70963 \end{array}$$

$$\begin{array}{r} 448 \\ 896 \\ 1792 \\ \hline 459 \end{array}$$

$$\frac{0.01094}{1.00085} = 0.01093$$

$$\frac{0.03465}{1.095} = 0.0316$$

$$\frac{0.05124}{1.117} = 0.0459$$

$$3465 : 1095 = 3164$$

$$\begin{array}{r} 4478 \\ 448 \\ 896 \\ \hline 5016 \end{array}$$

$$\text{stomach production: } \frac{3164}{1093} = \frac{4493}{5003}$$

$$z_y = \frac{0386}{4617}$$

$$\frac{459}{1093} = \frac{6618}{0386}$$

$$z_y = \frac{6232}{6232}$$

$$2895$$

$$4200$$

$$\begin{array}{r} 6232 \\ + 7782 \\ \hline 4014 \end{array}$$



Slyer 75% 6.2 149 251°  
 0.6523 0.3800 0.2803

23

65% 8.5  
 0.2221  
 8.5  
 49.82 0.0925

45.82 ~~4.6454~~ 1950  
 0.0512  
 37.5° 17°  
 0.01094

8145 5911 4477  
 1855 4089 5523

fl. 153 256 357  
 8.7 6.4  
 103:82= 101:67= 16.6  
 16 12 400 340

~~299 313 327 341 356~~  
~~17 18 19 20 21~~

286  
~~15 16~~

fl. 151	161	171	182	2.57	2.72	2.88	3.04	3.20	3.37	3.55
8 60	70	80	90	150	160	170	180	190	200	210

Slyer min 8.1 14.3 20.3  
 25.18 13.87 8.301  
 4011 1389 9193  
 5989 0611 0804

0.0394 0.0726 0.1204

332:6.2= 478:6

4 5.3 6.7 8.0 9.4

0.0  
 70 77 84 92 100 108 117

0.0390 432  
 80 90 10 11 12 13 14 15 16 17 18 19 20  
 4 44 49 53 58 62 67 72 76 8 84 88 93

$$\text{I). } g = \overset{20.204}{\cancel{7.2}} \quad \overset{0.552}{19.5} \quad \overset{0.906}{32}$$

$$\text{II). } g = 17.5 \quad 39.5 \quad \overset{98}{\cancel{65}} \quad 57 \quad 106 \quad 119$$

$$\text{III } g = 29 \quad 43.5 \quad 77.5 \quad 42 \quad 83$$

$$\begin{array}{r} 113 \\ 25.2904 \\ 32.4 \\ 220.30 \\ 2.214 = 7.0 \end{array}$$

$$\underline{0.0283. 72}$$

1

$$\begin{array}{r} 4518 \\ 8573 \\ \hline 3091 \end{array} \quad \begin{array}{r} 4518 \\ 2900 \\ \hline 7418 \end{array} \quad \begin{array}{r} 4518 \\ 5051 \\ \hline 9569 \end{array}$$

$$\begin{array}{r} \cancel{2837.845} \\ 802 \end{array} \quad \begin{array}{r} 8096 \\ 6734 \\ \hline 1362 \end{array} \quad \begin{array}{r} 8075 \\ 6734 \\ \hline 1341 \end{array}$$

$$\begin{array}{r} 1362 \\ 2430 \\ \hline 3792 \\ 4617 \\ \hline 0.239.60 \end{array} \quad \begin{array}{r} 1362 \\ 5966 \\ \hline 7328 \\ 2617 \\ \hline 0.540.60 \end{array} \quad \begin{array}{r} 1362 \\ 7559 \\ \hline 8921 \\ 7617 \\ \hline 0.780 \end{array} \quad \begin{array}{r} 1362 \\ 8129 \\ \hline 9491 \\ 4617 \\ \hline 0.889 \end{array} \quad \begin{array}{r} 1362 \\ 9912 \\ \hline 1274 \\ 4617 \\ \hline 1.34 \end{array} \quad \begin{array}{r} 1362 \\ 0253 \\ \hline 1615 \\ 4617 \\ \hline 1.45 \end{array} \quad \begin{array}{r} 1362 \\ 0755 \\ \hline 2117 \\ 4617 \\ \hline 1.63 \end{array}$$

$$\cancel{827} \quad 187 \quad 269. \quad 307 \quad 463 \quad 501 \quad 562$$

$$\boxed{0.01384 \quad 0.0212 \quad 0.0449 \quad 0.0512 \quad 0.0772 \quad 0.0835 \quad 0.0937}$$

$$\begin{array}{r} 1341 \\ 4624 \\ \hline 5965 \\ 4014 \\ \hline 1951 \end{array} \quad \begin{array}{r} 1341 \\ 6385 \\ \hline 7726 \\ 4014 \\ \hline 3712 \end{array} \quad \begin{array}{r} 1341 \\ 8893 \\ \hline 0234 \\ 4014 \\ \hline 6220 \end{array} \quad \begin{array}{r} 1341 \\ 9191 \\ \hline 0532 \\ 4014 \\ \hline 6518 \end{array}$$

$$\boxed{0.0157 \quad 0.0237 \quad 0.0428 \quad 0.0443}$$

225

$$0.89.2.89.$$

$$\begin{array}{r} 2316 \\ 26015 \\ \hline 2576 \end{array}$$

$$2.58.9 = 2.87$$

$$0.86.29 = 0.3$$





$I = h = 18.0 \text{ cm}$   
 $II = 18.0 (\text{Vacuum } 70 \text{ cm})$   


---

 $III = h = 39 \text{ cm}$   
 $IV = \text{Vacuum } 65 \text{ cm}$



26/4 1.04 12.10

$h = 8.5 \text{ cm}$   
 $I$

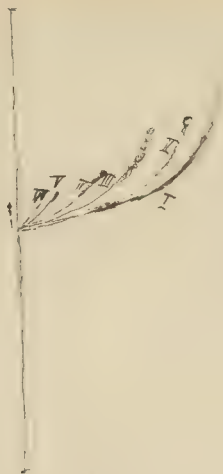


Vacuum 70, 10

$II, h = 18.0 \text{ cm}$   
 $12.43$



$I = 39 \text{ cm}$



$I = 33 \text{ cm}$

$III = 24 \text{ cm}$

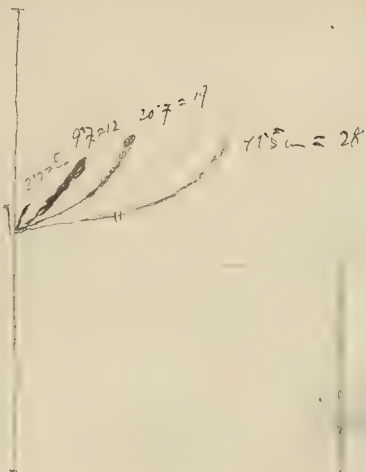
$IV = 16.5 \text{ cm}$

$V = 9.7 \text{ cm}$

$VI = 5.5 \text{ cm} = 95 \text{ kgpl. min.}$

$41.5 \dots 28 \text{ kgpl.}$

$h = 29 \text{ cm} \quad 20.5$



$$\frac{41.5}{20.7} = 2$$

$$28 : \sqrt{2} = 19.7$$

10

$$\frac{41.5}{27} : \frac{9.7}{8} = 4.28$$

$$\sqrt{4.28} = 2.06$$

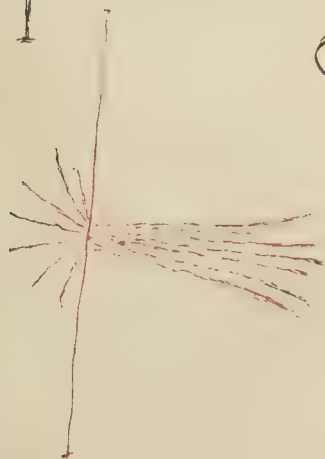
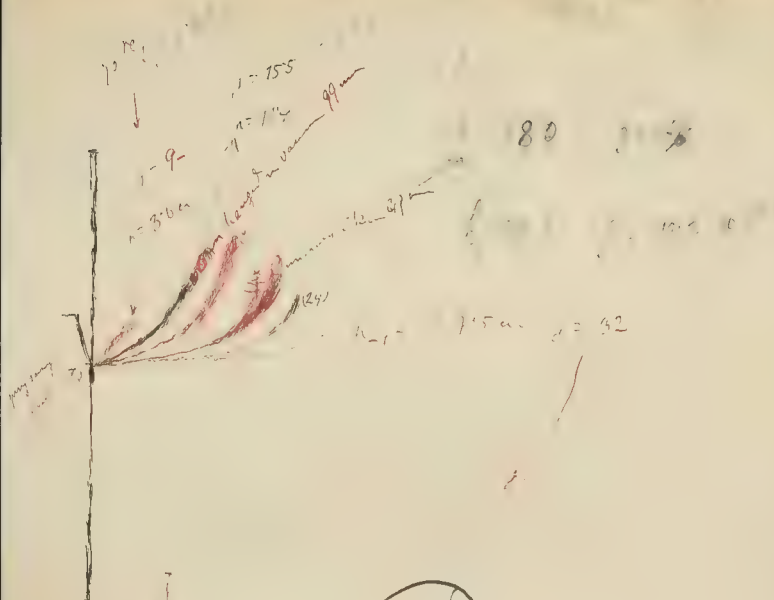
$$28 : 2.06 = 14$$

$$\sqrt{20} = 4.5$$

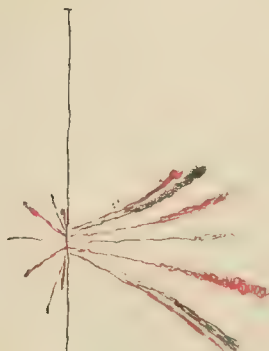
$$28 : 4.5 = 56 : 9 = 6.2$$

$h$	$g \text{ cm}$	$g \text{ ob. } \sqrt{k}$
41.5	28	
20.7	19	19.7
8.7	12	14
2.0	5	6.2





0.552



1-2.8

1-1.2

0.204

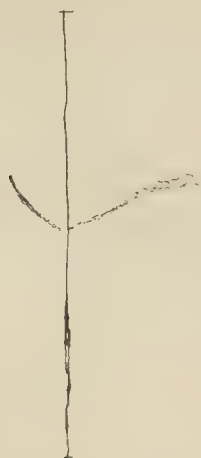
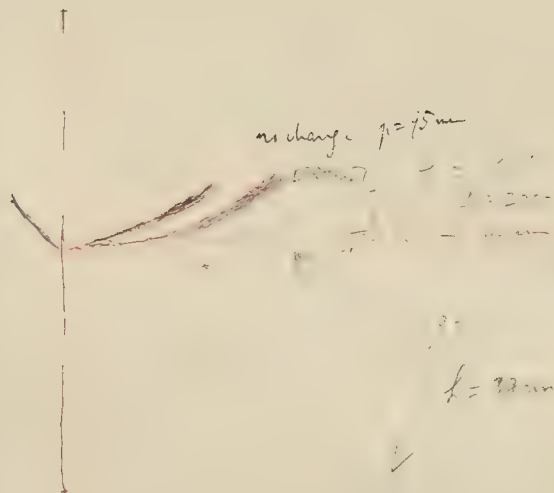
25



$\theta = 13.0^\circ$

25

29/1/81



I.  $k=92\text{mm}$

II = atm.

$f=5\%$

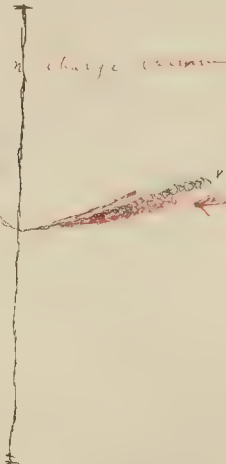
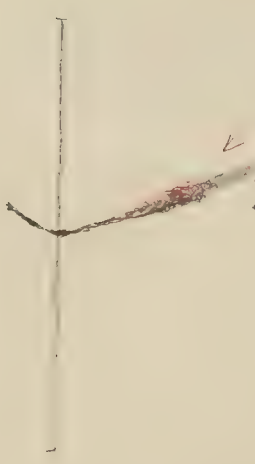
$k=71\text{mm}$

$k=71\text{mm}$

$k=71\text{mm}$

$k=71\text{mm}$

$k=71\text{mm}$



charge  $k=92\text{mm}$

$k=105\text{mm}$

$k=105\text{mm}$

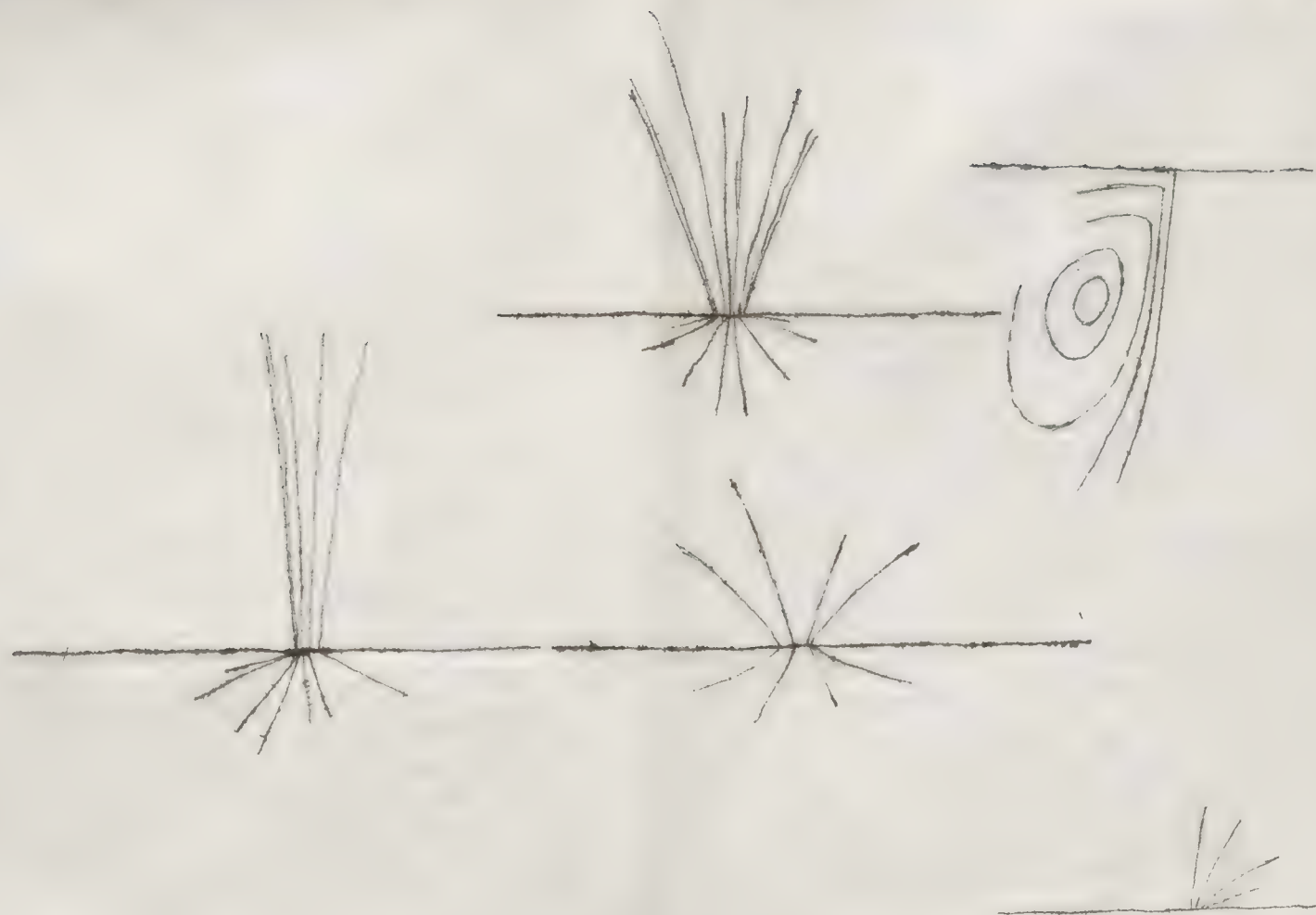
charge

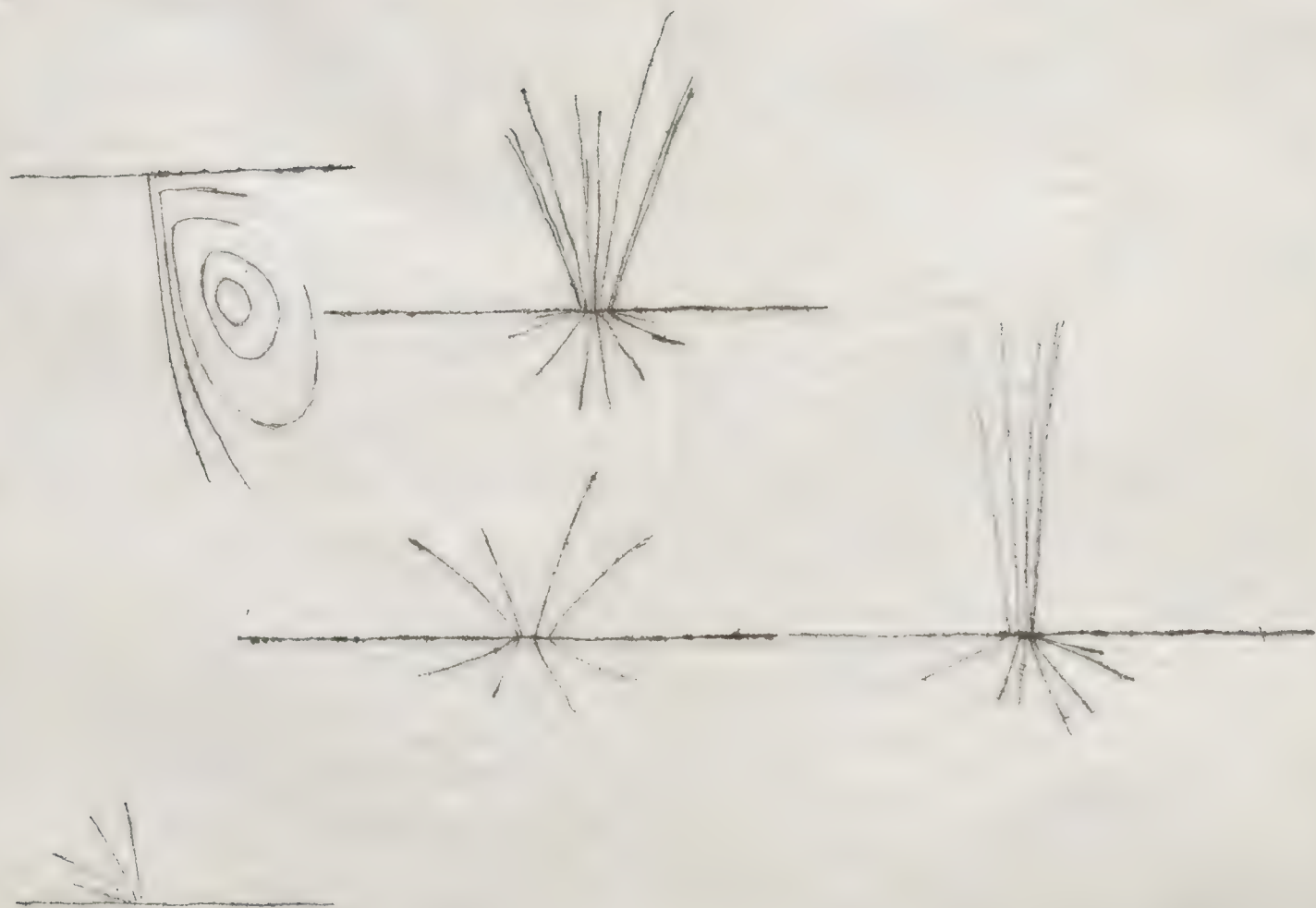
$k+1=11\text{mm}$

$k+1=11\text{mm}$

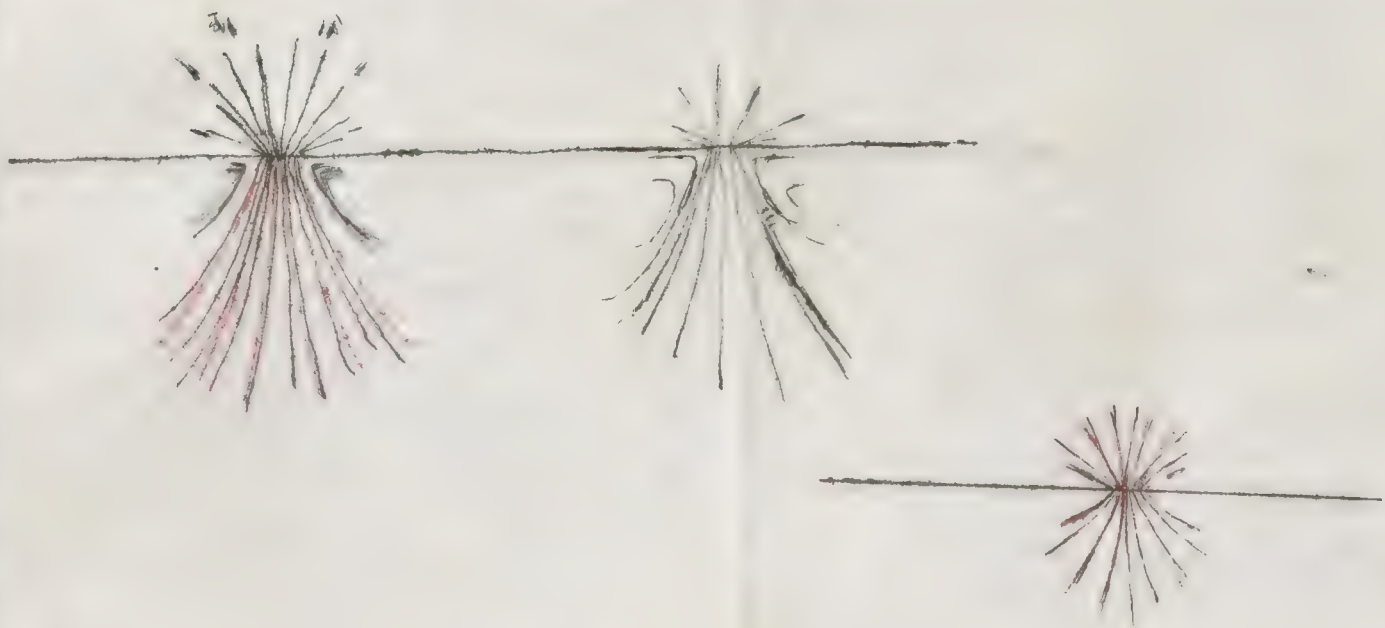
$q=5$

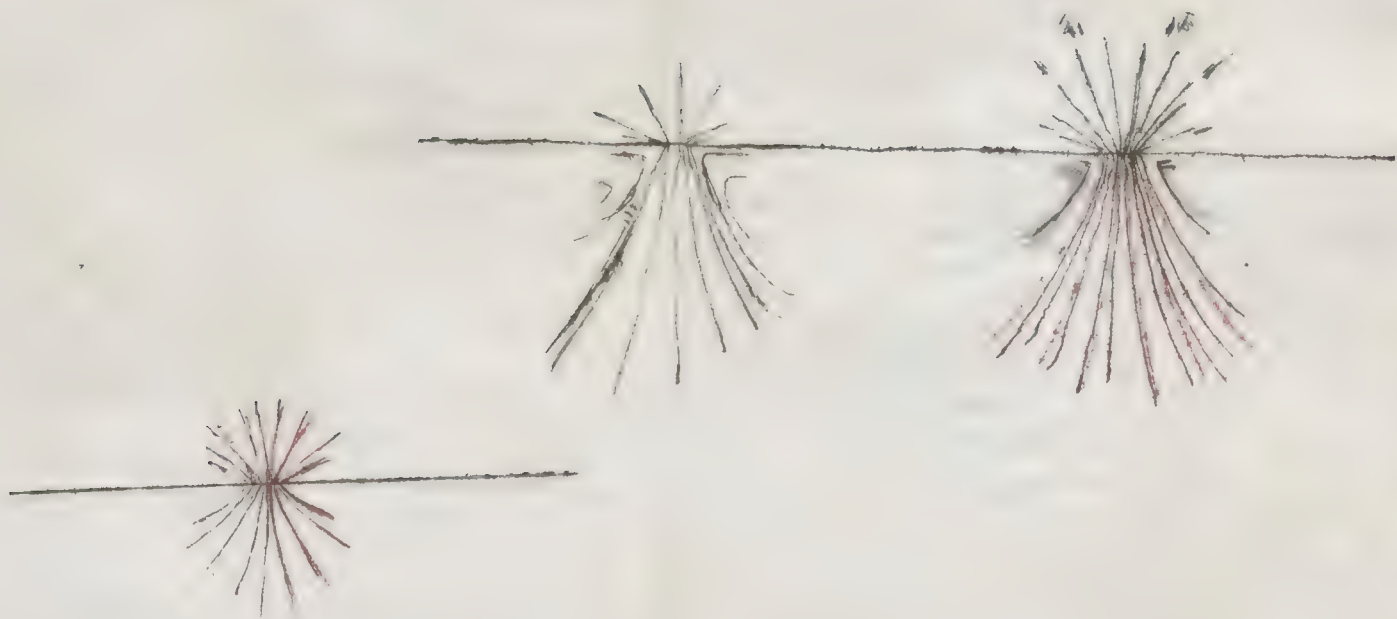














30/7 1962

15-18/62

(0.552)



4. 12

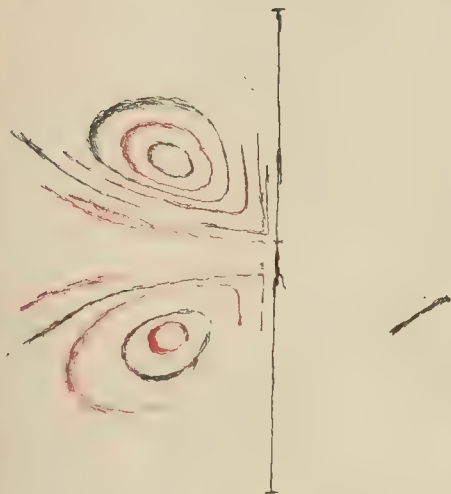
 $k = 3000$  $j = 73$

$$h = 4.8$$

$$g = 3.5$$

$$5.2 - 6.45$$

$$0.890$$



$$L = 1.8$$



26y. 90

29

57



$\frac{14.449}{32}$   
45  
15 49'  
13'

0.0449

0.0434

$$\theta_{\text{ref}} = 19.2$$

7.6 10<sup>20</sup>

$$\theta_{\text{E}} = 18.9 \quad 14^\circ$$

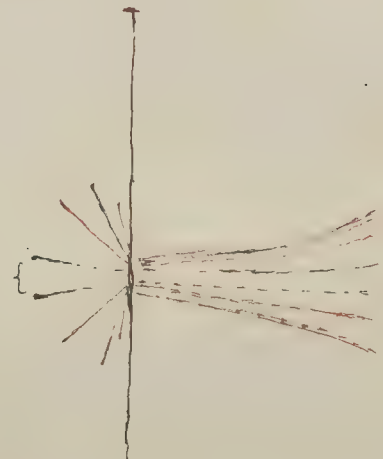


$$53 + \frac{5.79}{24.5} = 54$$

1 =

$$18 = 14^\circ$$

Sign



$$j = 106$$

0.0835

$d = 4.5$   
 $3.4$   
 $5.4$   
 $7.0$   
 $3.5$   
 $1.6$   
 $4.8$   
 $3.9$   
 $4.0$   
 $3.2$   
 $4.0$   
 $4.5:11$   
 $= 4.0$   
 $\frac{7.5}{2.5} = 3.0$

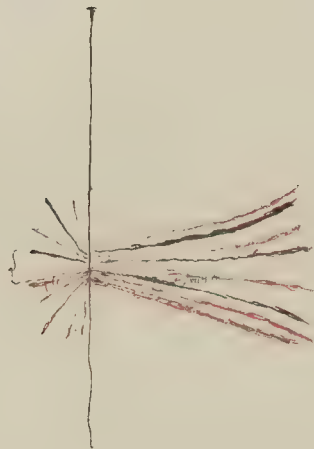


Fig. 66

Fig. 70

30

h-cc 1st 2nd



~~0.0449~~

$$\Delta = \frac{1.4}{32} = \frac{1.7}{76}$$

~~0.0812~~

$$\frac{11.7}{254}$$

0.0490

= corr.

~~0.0772~~

0.0756

corr

96...

96... 6/6



$\frac{1.6}{32}$

~~0.0312~~  
0.0296  
cm

$\frac{1.1}{32} .738$

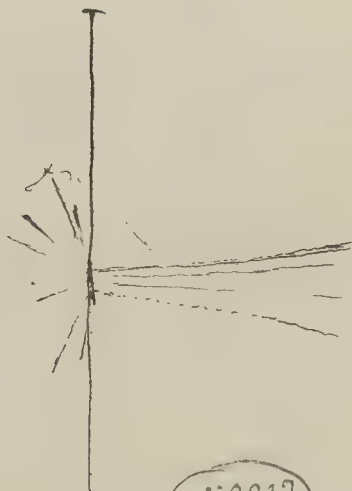
~~0.0158~~  
0.0134



7/6 5h

Vatun 47 cm

$g = 119$



7/6 4h

$\theta_c = 19.5$

$g = 63$



$\theta_c = 10.6$   
 $\theta_c = 19.5$   
 $\theta_c = 19.5$





$\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$

$\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$

$\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$

$\frac{309618}{12}$   
 $25801.5$

$\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$   
 $\frac{11725}{1.5}$

$\delta = 20^\circ$

32

$\frac{27.025}{0.443}$   
 $\frac{20.582}{1.785}$   
 $\frac{93}{93}$   
 $\frac{20.950}{0.173}$   
 $\frac{18.797}{1.095}$

3200  
 rozszerzenie  
 wody ziemnej

$7/6 \quad 12^h 30$

u wrotach

u wrotach :  $237''$   $239''$   
 det.  $20^\circ$   
 pow.  $95^\circ$

$34 \quad 31'$

$\frac{47' 27''}{59' 42''}$   
 $\frac{19' 4''}{12' 15''} = 735''$

$735 : 238 = 3.09$   
 $\frac{2781}{155} \cdot 1.095$   
 $3384 =$

$\frac{1.095}{1.095}$   
 $\frac{3384}{3384}$

$$n = A \frac{t_0 - t}{t - T}$$

$$\frac{1}{A} \ln \frac{T_0 - t_0}{T_0 - t_1}$$

$$\frac{1}{A} \ln \frac{T_0 - t_1}{T_0 - t_2}$$

$$\frac{1}{A} \ln \frac{T_0 - t_1}{T_0 - t_2} = \frac{t_1 - t_2}{T_0 - t_1}$$

$$\frac{1}{A} \ln \frac{T_0 - t_1}{T_0 - t_2} = \frac{t_1 - t_2}{T_0 - t_1}$$

$$\frac{1}{A} \ln \frac{T_0 - t_1}{T_0 - t_2} = \frac{t_1 - t_2}{T_0 - t_1}$$

$$\frac{1}{A} \ln \frac{T_0 - t_1}{T_0 - t_2} = \frac{t_1 - t_2}{T_0 - t_1}$$

$$\frac{1}{A} \ln \frac{T_0 - t_1}{T_0 - t_2} = \frac{t_1 - t_2}{T_0 - t_1}$$

$$\frac{1}{A} \ln \frac{T_0 - t_1}{T_0 - t_2} = \frac{t_1 - t_2}{T_0 - t_1}$$

6.2	0.652	21620	18110	12.7	2.3
10.4	0.780	50000	10000	256	3.2
21.1	0.280	100000	357		

$$0.552 =$$

$$0.295$$

$$0.552 : 0.091 = 6.07 :$$

$$0.049$$

on the ... 47.3

0.2 - 0.8

$$46.8\%$$

$$x \cdot 96 + a \cdot 378 = y \cdot 46.8 \quad 53.2$$

$$x \cdot 4 + a \cdot 62.2 = y \cdot 53.2 \quad 46.8$$

$$x = a \frac{62.2 \cdot 46.8 - 37.8 \cdot 53.2}{96 \cdot 53.2 - 4 \cdot 46.8}$$

$$= a \frac{62.2 - 37.8 \frac{53.2}{46.8}}{96 \frac{53.2}{46.8} - 4}$$

$$53.2 : 46.8 = 1.137$$

$$\begin{array}{r} 640 \\ 172 \\ 32 \end{array}$$

$$\begin{array}{r} 96 \cdot 1.137 \\ 10233 \\ 2822 \\ 10915 \\ - 4 \end{array}$$

$$\begin{array}{r} 378 \\ 378 \\ 1134 \\ 2040 \\ 4298 \end{array}$$

$$\begin{array}{r} 62.2 \\ 430 \\ 19.2 : 105.2 = 0.183 \\ 87 \\ 3 \end{array} \quad x = a \cdot x$$

$$\begin{array}{r} 9001 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \end{array}$$



$$\frac{P}{u} = \frac{1}{2} \left( \frac{1}{u} \right)^2$$



$$\mu = \frac{1}{2} \frac{1}{u}$$

$$1 = \frac{1}{2} \frac{1}{u}$$

1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000

$$1.000000$$

$$1.000000$$

$$\frac{1.000000}{1.000000} = 1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

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$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

$$1.000000$$

1000 1000

726.5

2814.0

$$\begin{array}{r} 2077^5 \cdot 43 \\ \hline 57 \end{array}$$

83100

62325

84.1 25

323

383

478

1

77660

1792

1567;

35

1269.0

1987

102 0'3 : ~~47~~  
210 43 = 2489'0

210

3 1 3

39

$$\frac{2x^2}{x^2 + 2}$$

1562. 2.5

1582 + 21553 + ~~21553~~

77-22

$$4^2 \cdot \frac{4}{4} =$$

Tr. 24-06

64-55

100

250  
3644

5616

~~1207  
107  
107  
107  
107  
107  
107~~

19507

93702

— 570 —

100

95.415%

67511

5 2 2 2

1970

2257

4. 3. 4

75 642

54.45

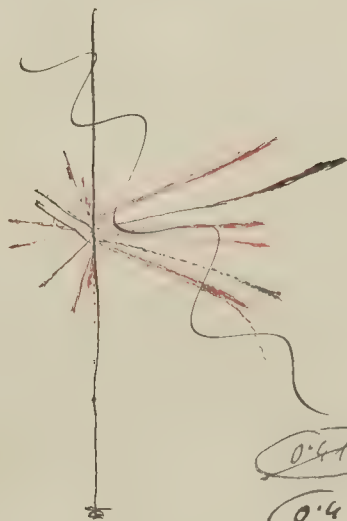
1917



(2) 14/6  
1<sup>h</sup> 35

$g = 77.5$  narrow

$\theta = 178$



0.418

0.423

34

$g = 48.5$

(0.237)

~~0.237~~  
~~0.237~~



$d_{20}^{\text{20}}$  20.5, 10.0

11/6 7<sup>h</sup>30 4<sup>h</sup>22

g<sup>202</sup>

$\theta_2 = 19.2$

47 7.4199  
 46 92  
 45 95  
 44 98  
 43 10.41  
 42 64  
 41 94  
 40 10  
 35 08.75  
 30 07.40  
 25 06.10

6.2. 0.6513

2.2. 50-45%

4.0. 2.5: 0.2221 3466  
 4.0. 2.5: 0.2221 6534  
 4.0. 2.5: 0.2221 0661  
 4.0. 2.5: 0.2221 0239

0492 9508 773

H<sub>2</sub>O: 16 5.0. 1.0. 5.0.  
 16 10.0. 3.0.  
 16 10.0. 3.0.  
 16 10.0. 3.0.  
 16 10.0. 3.0.  
 16 10.0. 3.0.  
 16 10.0. 3.0.  
 16 10.0. 3.0.  
 16 10.0. 3.0.  
 16 10.0. 3.0.  
 16 10.0. 3.0.

0068 9932 775



0.0227  
 0.225

0.2. 217

2.5. 1.0. 5.0.  
 2.5. 1.0. 5.0.  
 2.5. 1.0. 5.0.  
 2.5. 1.0. 5.0.

$\theta = 20.3$

25.240

2.5. 1.0. 5.0.  
 2.5. 1.0. 5.0.

2.5. 1.0. 5.0.  
 2.5. 1.0. 5.0.

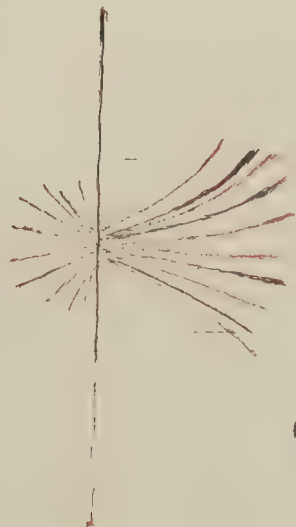
2.5. 1.0. 5.0.

1/2

$g = 93$

7

$\theta_c = 14.1^\circ$



0449

0443

1/4  
28

11.5

$g = 20$

11.5

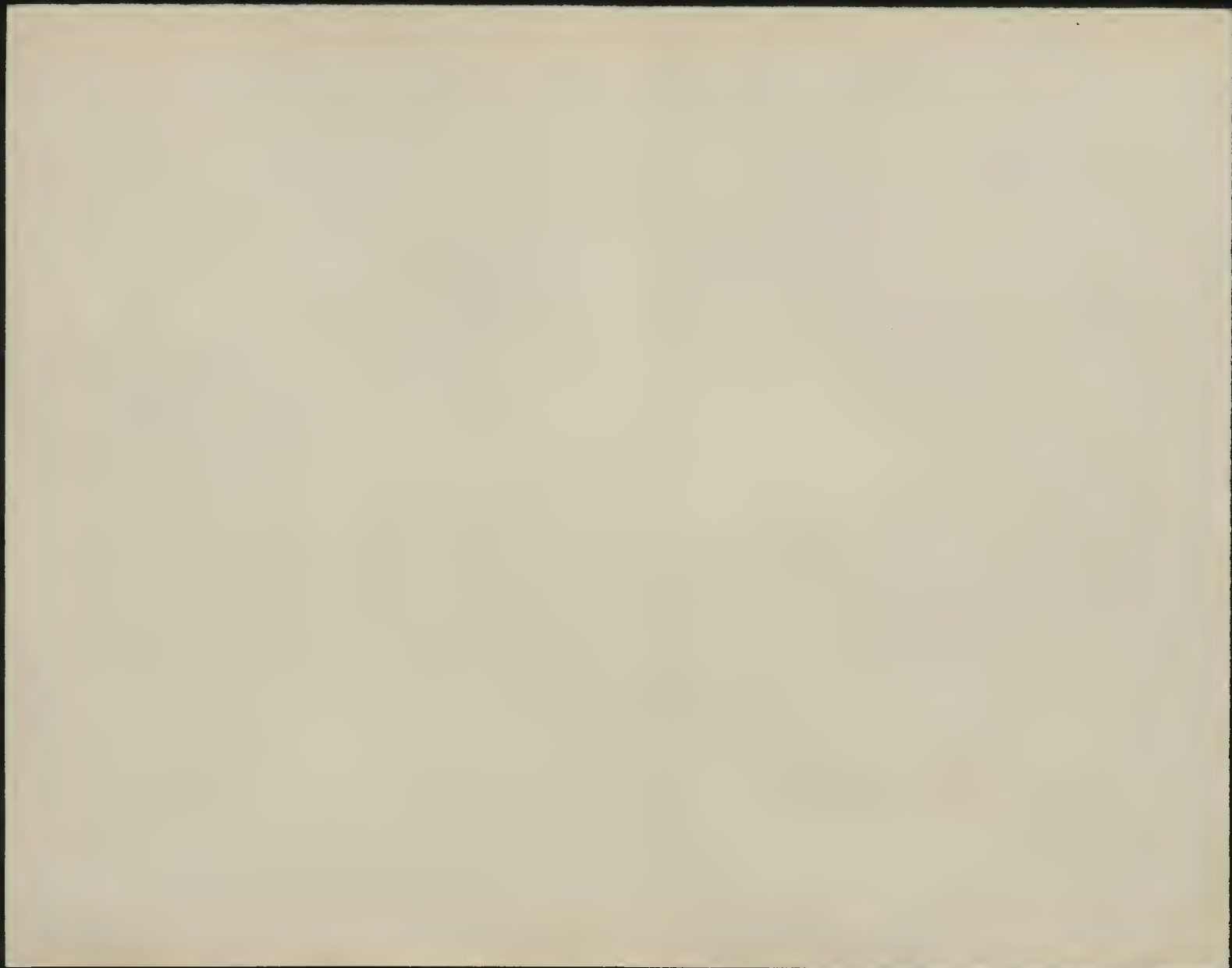
$g = 29$



0157

11.5



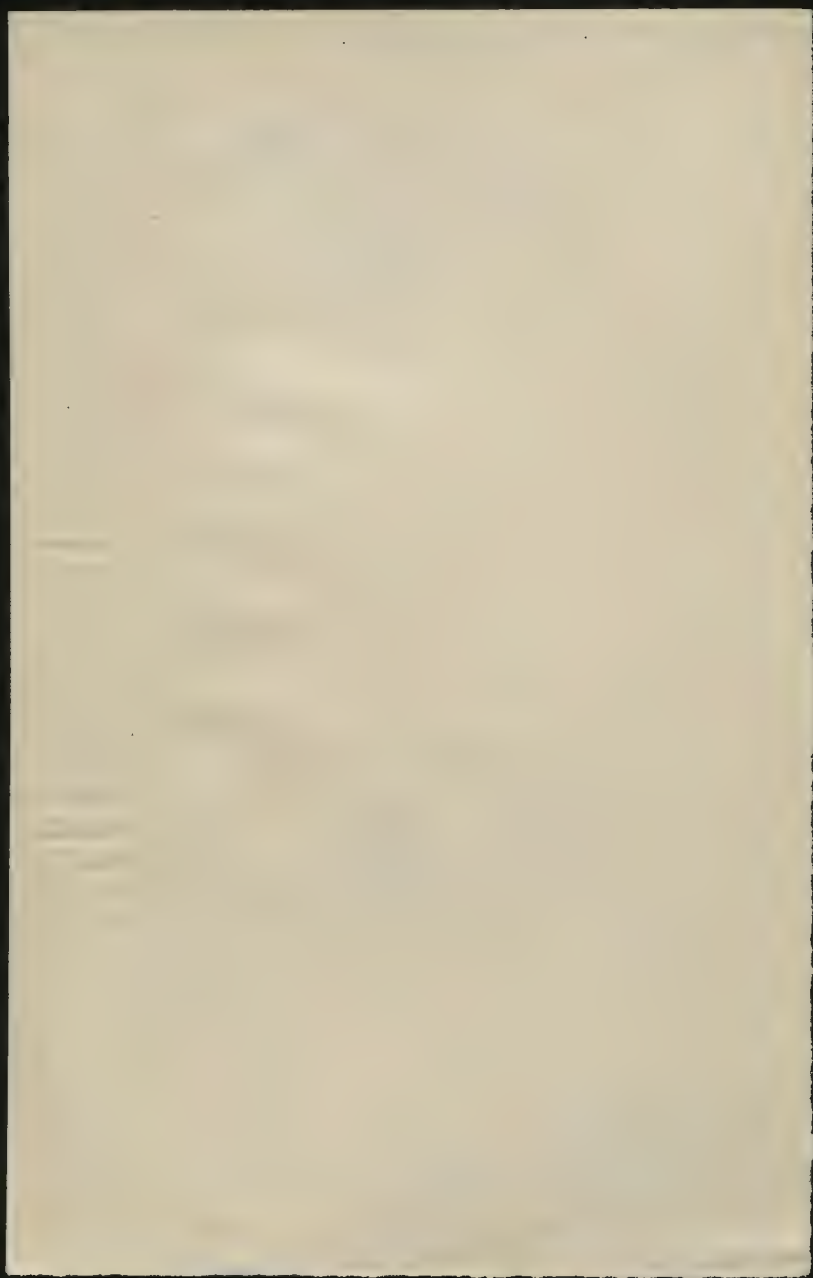


$$\frac{10' 46''}{27' 15''}$$

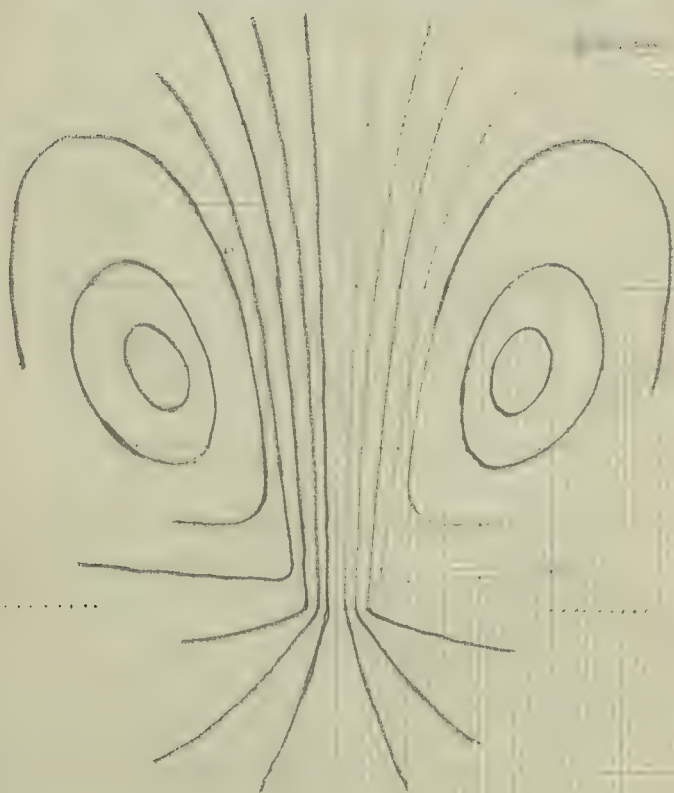
1021

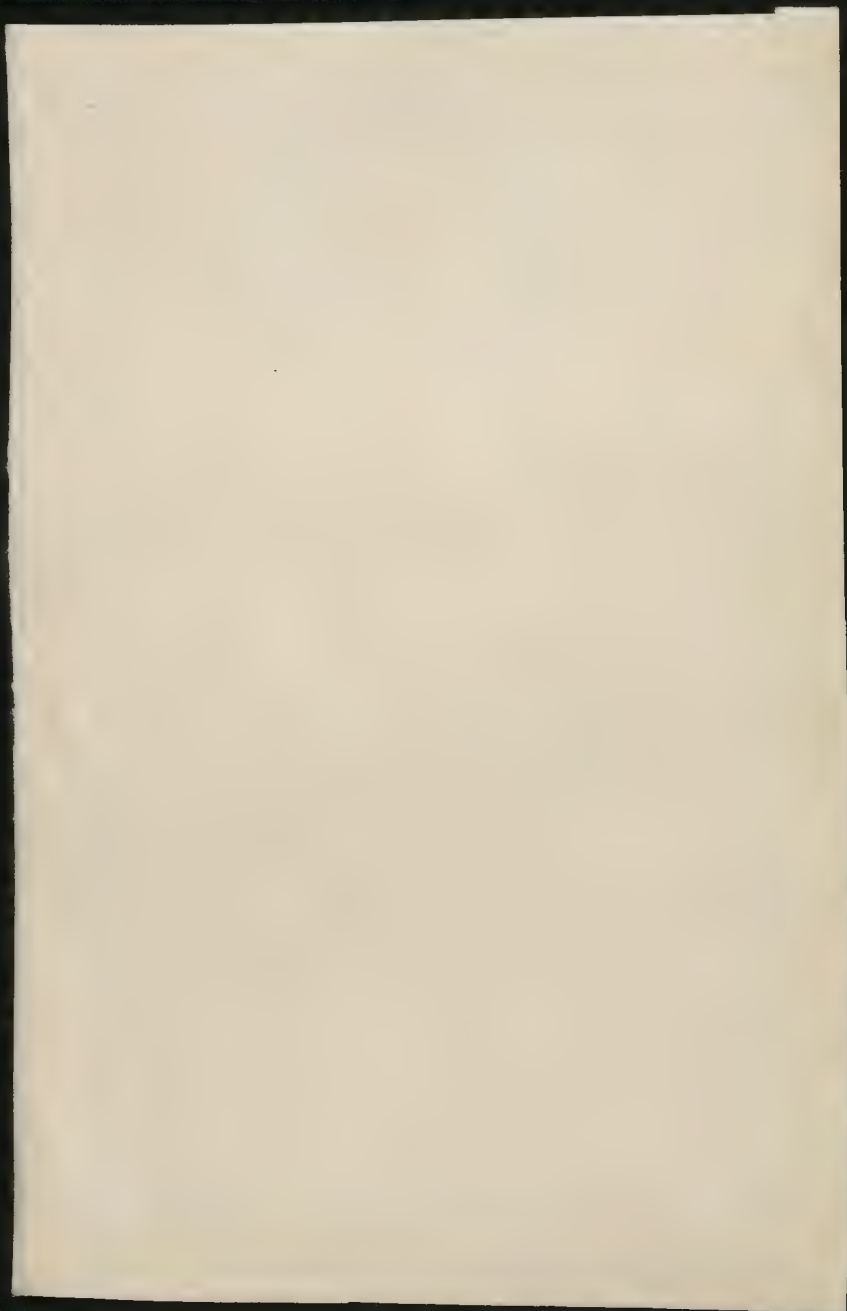
F. 1. 100

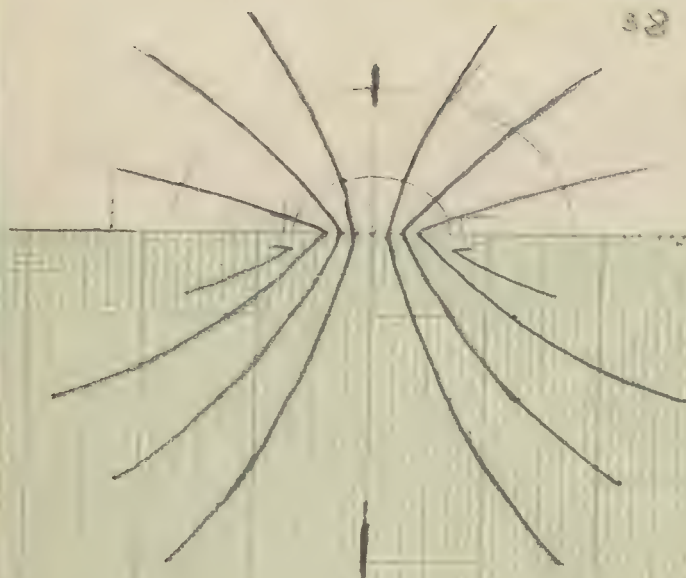
1088 : 221



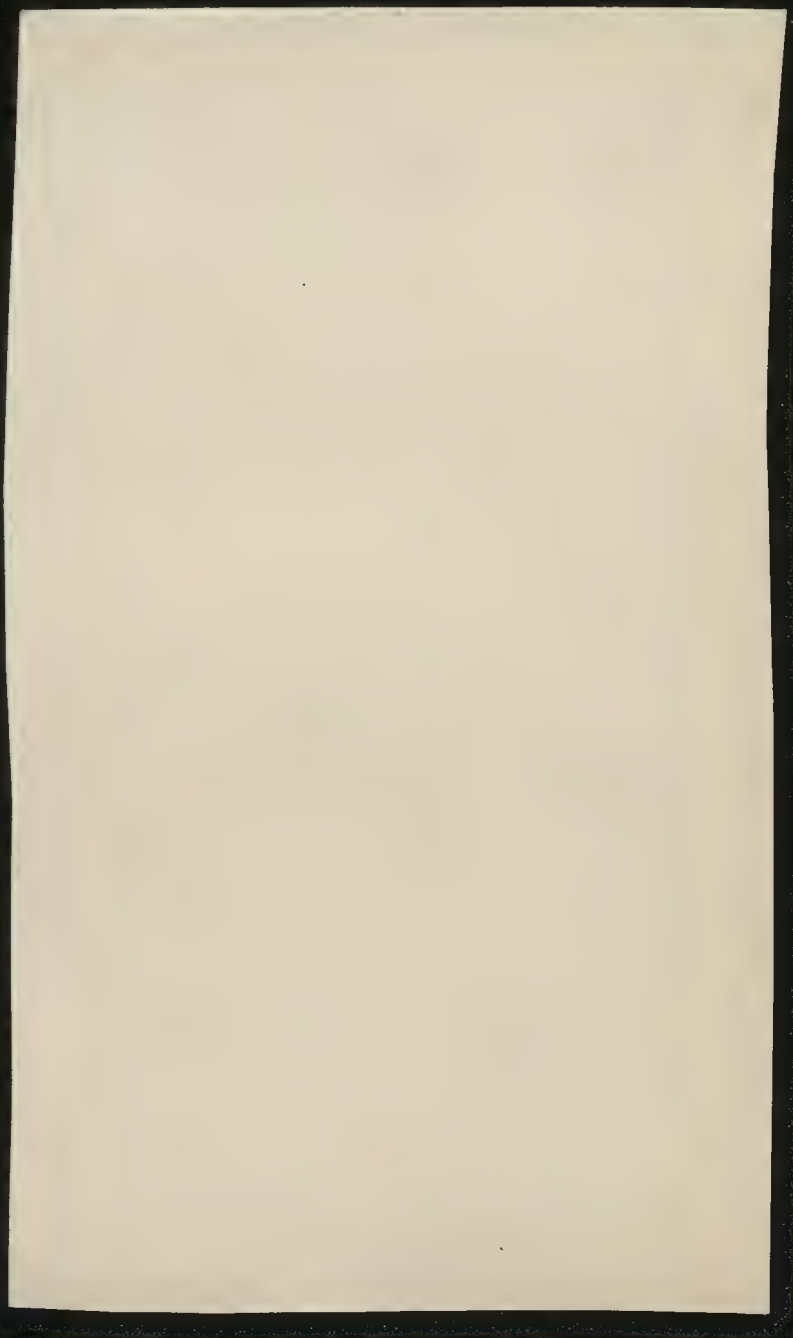


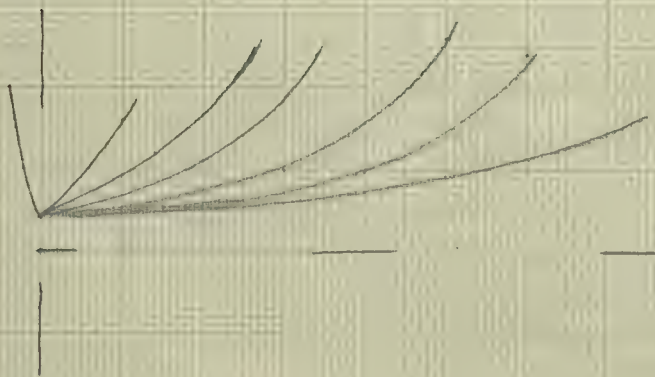
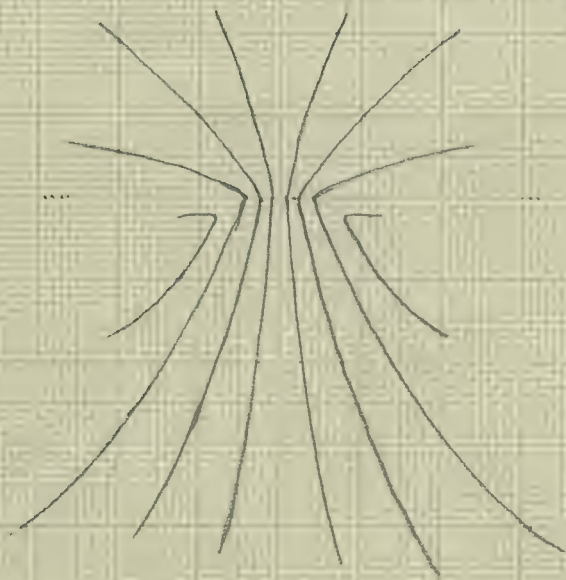


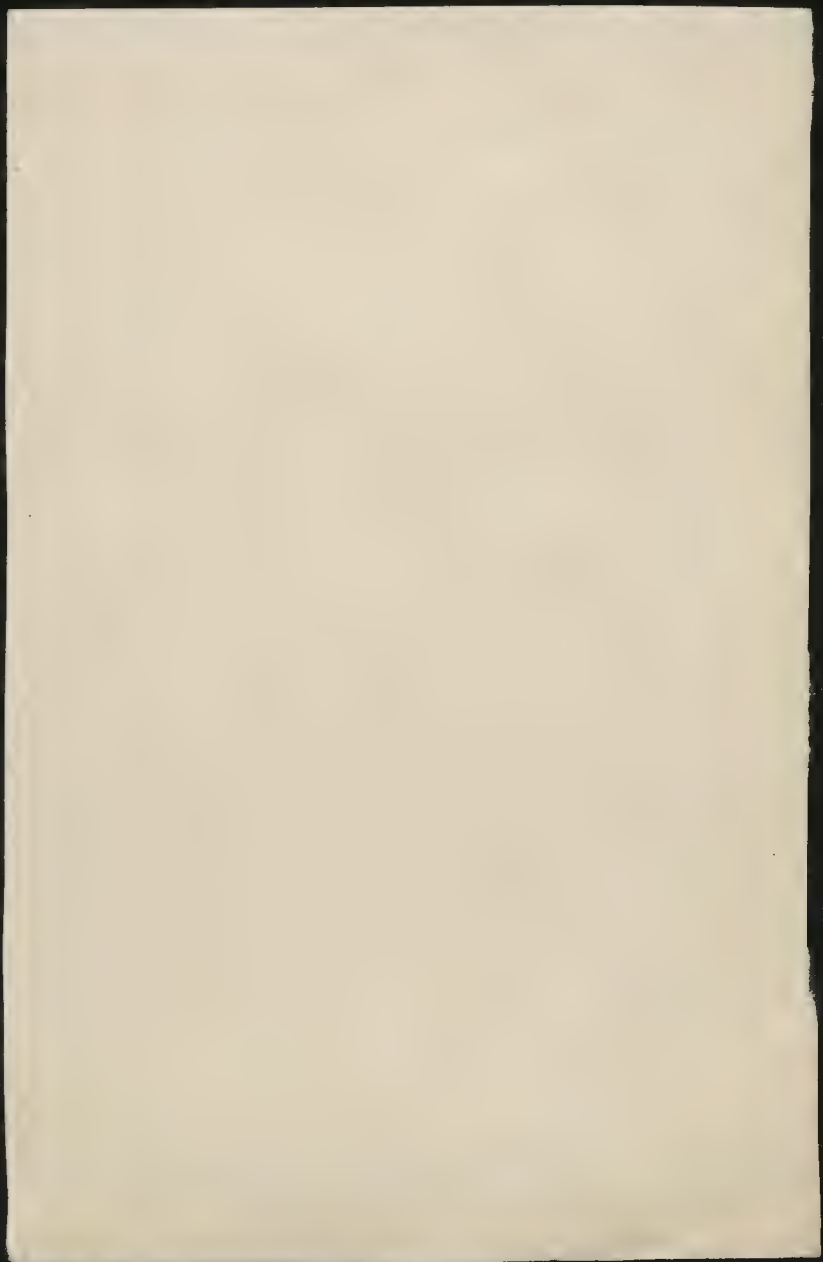














$$\frac{16}{12.8} = 1.00085$$

$$57.3:85 = 4.4$$

total 4.4 mag only

12.8

remaining: 1.16 %

17.5

-5.4 -0.2 12.2  
 10.6 -0.2  
 14.4 -0.6  
 14.2 -0.2

20.1 -6.1  
 0.0 -6.2  
 -0.2 -6.1  
 -0.3

-3.1

15.38 -7.4  
 15.5257

25.25

25.248

-10.8 -0.6  
 -15.2 +0.4

-13.1 +0.2

-13.0 12.9 +0.4  
 25.514

+7.8 0.0

7.6 0.2

7.4 0.2

25.316 +7.16

+3.8

$$10:1:0 = 1.7 \text{ mag}$$

25.321

25.2965

25.75

0.0 -16.5

-0.4 -16.3

0.7 -16.0

-1.1

-8.4

-0.5

25.265

$$1.0775:1.00085 = 1.00396$$

0.0037

1.00373

$$\delta = 0.0745$$

(8.0+)

6.2+

0.3+

0.3+

2.2+

8.2-

5.2-

0.2-

3.2-

0.2-

165

252692

$\Delta = 0.076$

25270

252533

5.2

4.3+

25255

(0.5+)

0.0

0.0

0.0+

0.0+

0.6

5.6+

0.6+

0.01+

(0.5+)

5.5

5.5

5.5

5.5

3.5+

0.0+

0.0+

0.0+

2.0+

2.0

6.0

6.0+

0.4+

0.0+

5.4+

4.2+

4.2+

5.2+

0.3+

0.2

25274

25274

2.4

11.4

2.8

11.2

3.4

11.0

3.4

11.2

2.9

7.05

2 = 1mg

$-10.6$      $-1.1$      $25.25$   
 $-10.8$      $-0.2$   
 $-10.2$      $-0.6$      $25.255$   
 $-10.6$      $-1.0$   
 $-10.4$      $-1.4$      $(-5.08)$   
 $-10.6$      $-1.0$      $25.275$

$-8.7$      $-0.6$

$-8.3$      $-1.0$

$-8.4$      $-1.3$

$-8.0$

$-8.9$

$-1.0$

$25.2725$

$\Sigma 17.5$

$\Sigma 16.7$

$25.27$   
 $+0.1$      $-0.6$      $-6.0$      $41.$   
 $+0.1$      $-1.1$      $5.8$      $-0.2$   
 $+0.1$      $-1.0$      $5.7$   
 $-0.2$      $-1.1$      $-2.95$   
 $-0.3$      $-1.0$   
 $-0.6$      $(-3.3)$      $25.2585$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

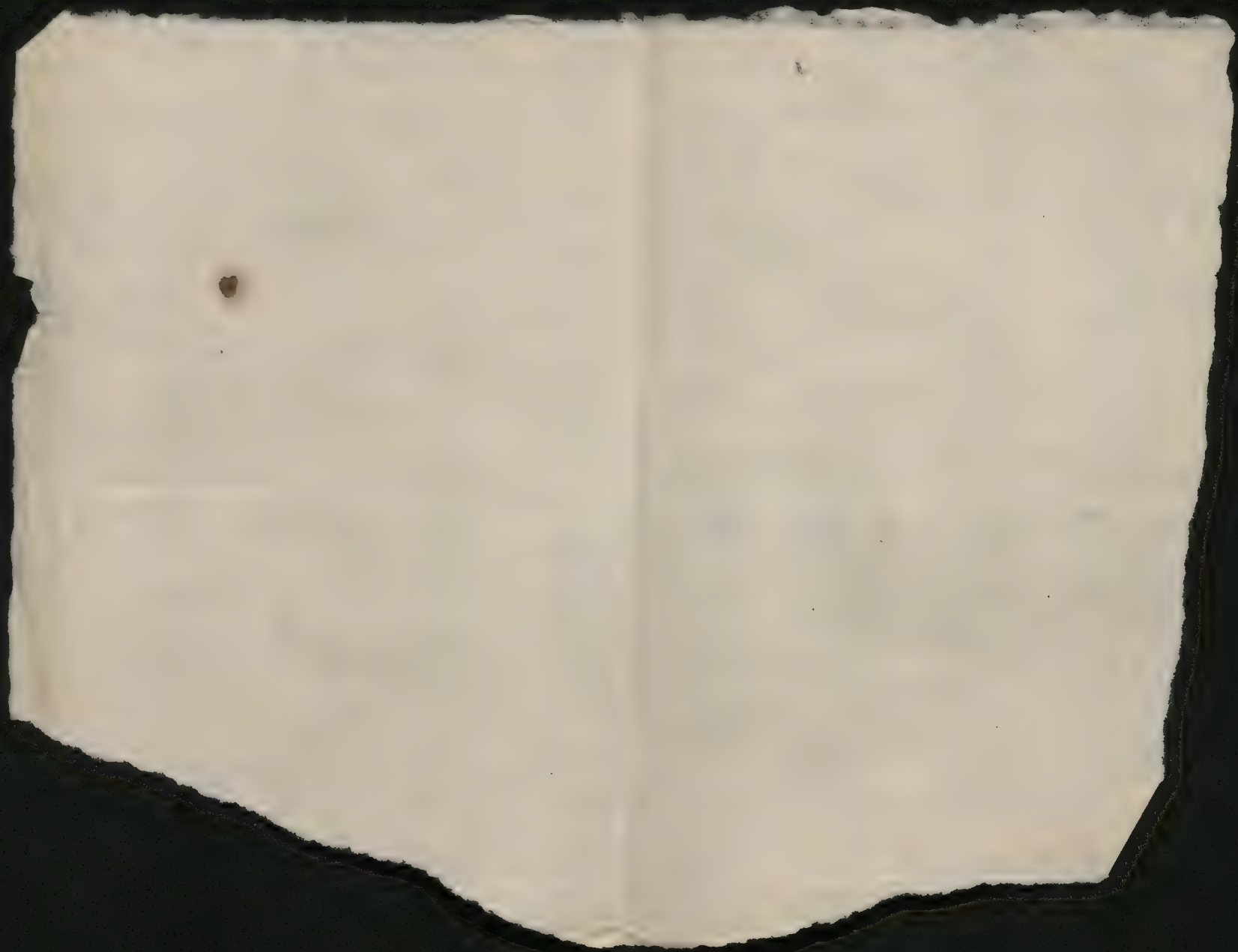
$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$

$+0.1$      $-1.1$





$+2.8$      $1.9$      $1.8$      $7$   
 $-4.7$      $4.9$      $1.8$

$25.750$   
 $-4.2$

$-2.8$      $1.9$      $1.8$   
 $4.9$      $1.0$

$27.015$      $-1.4$

$4.9$      $2.0$      $1.2$   
 $1.9$      $1.0$

$27.011$

$1.9$      $1.0$      $1.2$   
 $1.9$      $1.0$

$27.011$

$27.015$      $4.575$   
 $6.443$      $1.443$   
 $10.572$      $11.222$   
 $14.05$      $1.11$   
 $7.3$

$29.564$   
 $6.443$

$23.121$      $11.222$      $=$      $12.295$

$7.577$

$5.51$

$1.74$

$2$

$12.295$

$1.443$

*(Faint handwritten notes and calculations, possibly related to the above text.)*





$-12.5$      $-0.5$      $25.25$   
 $-1.0$      $-0.5$   
 $-9.5$   
 $-12.8$      $-0.5$

$25.25 - 7.7 = 17.55$

$-3.4$      $-0.5$      $25.25$   
 $-2.5$      $-0.5$   
 $-3.0$      $-0.5$      $25.25$   
 $-1.5$      $-0.5$

$-2.9$

$-1.7$

$3.4$      $+0.1$      $25.25$   
 $-3.3$      $-0.3$   
 $-3.2$      $-0.3$      $25.2494$   
 $-3.3$      $-0.3$   
 $-3.3$      $-0.3$

$25.263$

$26.2$

$26.24$

$25.2625$

$25.2541$

$25.2594$

$25.264$

$25.2694$

$25.2550$

$\Delta = 0.0125$

$-12.5$

$-1.0$      $-0.5$      $25.25$   
 $-1.0$      $-0.5$   
 $-1.0$      $-0.5$   
 $-1.0$      $-0.5$

$-7.4$

$25.264$

$1.1$      $+0.5$

$1.1$      $+0.5$

$1.1$      $+0.5$

$1.1$      $+0.5$

$1.1$      $+0.5$

$1.1$      $+0.5$

$1.1$      $+0.5$

$1.1$      $+0.5$

$1.1$      $+0.5$

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$1.1$      $+0.5$

$1.1$      $+0.5$

$1.1$      $+0.5$

$1.1$      $+0.5$

$-2.5$

$-1.5$      $+0.7$

$-2.5$

$25.263$

$25.251$

$25.252$

$25.256$

$-25.24$

$25.256$

$25.262$

$25.250$

$25.2494$





1000  
+ 2.6

2.8

- 3.0

+ 2.8

+ 10.4

10.4

+ 10.25

10

13.0

- 3.6

+ 6.5

3.011 - 1.8

1.2

1000

+ 0.1

- 1.2

- 1.1

- 0.1

3.1

- 0.1

1.1

- 0.1

- 0.2

0.2

- 1.1

- 1.1

1.1

- 1.1

+ 0.2

7.1

+ 0.1

6.1

- 0.1

6.1

- 0.1

6.1

- 1.1

1.1

- 1.6

- 2.1

- 2.25

$\theta = 20.9^\circ$

58500

By hand

- 2.1 + 1.4

- 2.1 + 1.4

- 1.6

- 2.0 - 1.2 - 0.4

1.1

- 3.9 0.0

- 3.7

- 3.8

- 1.9

- 1.9 + 0.1

- 1.8 0.0

- 1.6

- 1.77 + 0.05

24.220

24.221

- 0.85 Euro

-5  
-112  
-112  
-112  
-112  
-112

+12  
-112  
-112

-112  
-112

112

-112  
-112

-112  
+24

-112  
-24

-112  
-112

-0.6  
+112

-0.6  
7.0

0.2  
112

-0.6  
112

-0.6  
112

-0.6  
112

-0.6  
112

-112  
112

-112  
+112

-112  
-112

-112  
112

-112  
10.0

-112  
9.7

-112  
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112

-112  
112

25.227

-5.8  
+12.0

-5.8  
+12.0

-5.8  
+12.0

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+12.0

-5.8  
+12.0

-5.8  
+12.0

25.229

25.229

25.229

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25.229

25.229

25.229

25.229

25.229

25.229

25.262

25.262

25.262

25.262

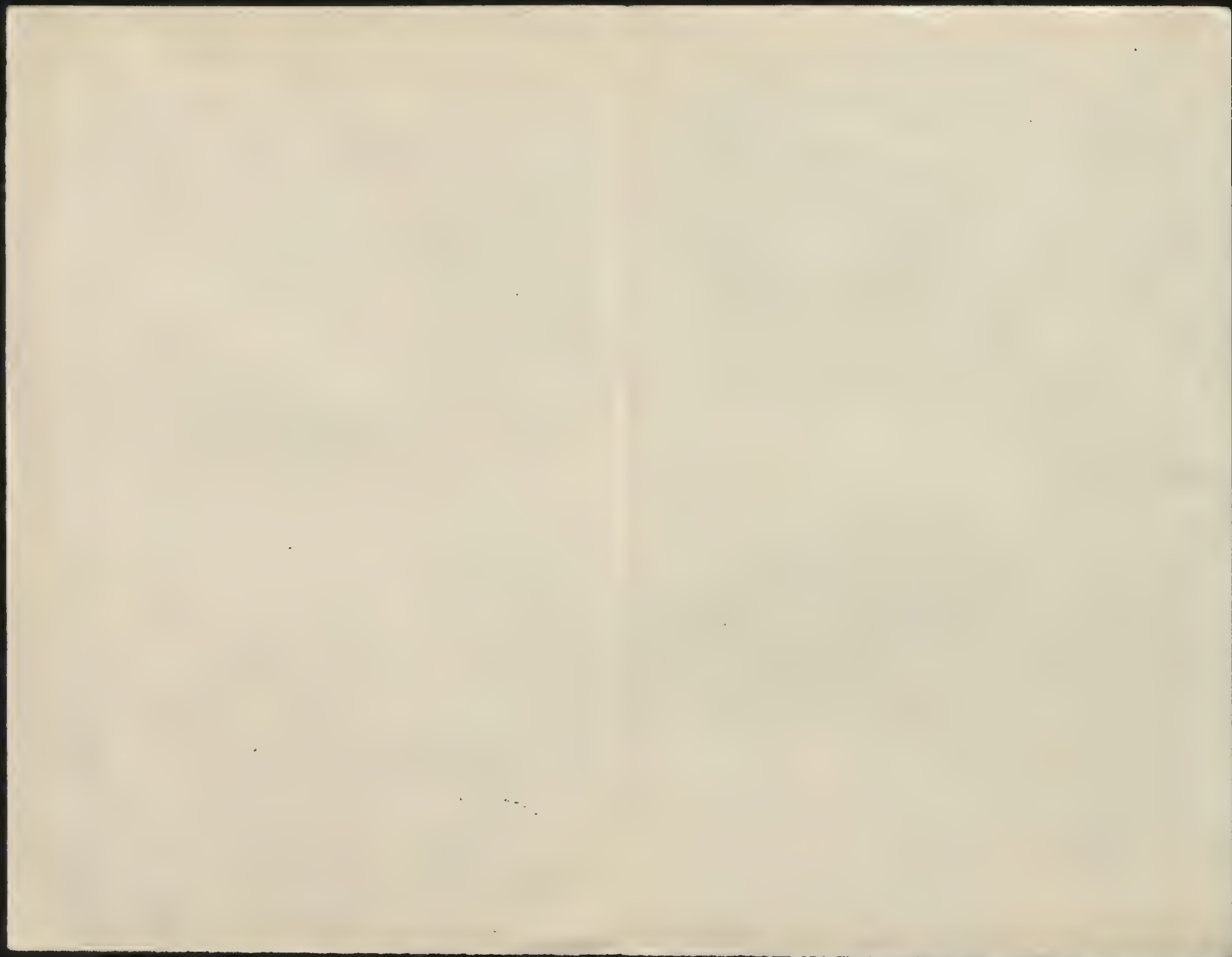
25.262

25.262

25.262

25.262

25.262





Sy. line / y. line only 40.5"

$$\begin{array}{r} 25'27.5 \\ 6'8.4 \\ \hline 18'87.9 \end{array} : \begin{array}{r} 25'27.5 \\ 6'8.4 \\ \hline 18'09.4 \end{array} =$$

$$1 + \frac{22}{1887.4}$$

1.0015

$$1 + \frac{29}{102} = 1.2843$$

1.00154

Section 9% 10' 10' 1.00701

$$\frac{15}{100} = 0.15$$

$$1.00701 - 0.15 = 0.85701$$

$$\frac{0.85701}{1.00701} = 0.85092$$

4

$$\begin{array}{r} -1.1 \\ -1.2 \\ -1.3 \\ -1.4 \\ -1.5 \end{array} \quad \begin{array}{r} +3.1 \\ 2.6 \\ 2.1 \\ 1.6 \\ 1.1 \end{array} \quad \begin{array}{r} 25'25.1 \\ 25'22.7 \\ 25'20.3 \\ 25'17.9 \\ 25'15.5 \end{array}$$

$$\begin{array}{r} -0.1 \\ -0.2 \\ -0.3 \\ -0.4 \\ -0.5 \end{array} \quad \begin{array}{r} +1.1 \\ 1.0 \\ 0.9 \\ 0.8 \\ 0.7 \end{array} \quad \begin{array}{r} 25'22.7 \\ 25'20.3 \\ 25'17.9 \\ 25'15.5 \\ 25'13.1 \end{array}$$

$$\begin{array}{r} -0.1 \\ -0.2 \\ -0.3 \\ -0.4 \\ -0.5 \end{array} \quad \begin{array}{r} +0.1 \\ 0.0 \\ -0.1 \\ -0.2 \\ -0.3 \end{array} \quad \begin{array}{r} 25'27.5 \\ 25'27.5 \\ 25'27.5 \\ 25'27.5 \\ 25'27.5 \end{array}$$

$$\begin{array}{r} +0.2 \\ +0.3 \\ +0.4 \\ +0.5 \\ +0.6 \end{array} \quad \begin{array}{r} 12.5 \\ 12.5 \\ 12.5 \\ 12.5 \\ 12.5 \end{array} \quad \begin{array}{r} 6.40 \\ 6.40 \\ 6.40 \\ 6.40 \\ 6.40 \end{array}$$

$$\begin{array}{r} 1.7 \\ 1.8 \\ 1.9 \\ 2.0 \\ 2.1 \end{array} \quad \begin{array}{r} 12.5 \\ 12.5 \\ 12.5 \\ 12.5 \\ 12.5 \end{array} \quad \begin{array}{r} 6.40 \\ 6.40 \\ 6.40 \\ 6.40 \\ 6.40 \end{array}$$

$$\begin{array}{r} -5.8 \\ -5.9 \\ -6.0 \\ -6.1 \\ -6.2 \end{array} \quad \begin{array}{r} 13.5 \\ 13.4 \\ 13.3 \\ 13.2 \\ 13.1 \end{array} \quad \begin{array}{r} 6.40 \\ 6.40 \\ 6.40 \\ 6.40 \\ 6.40 \end{array}$$

Wade

-12.0 7.0

11.7 8.0

11.7  
-11.9

berick -9.7

25.250

(25.244)

11.7 8.0

-1

-1

11.7  
-11.9

berick 2.710

2.9

-2.3 0.0

-2.2 -0.1

-2.3

-1.1

25.276

(25.275)

11.7

-0.8 +2.0

-0.6 1.9

-0.6

25.247

24 93

1231 : 241 = ..

$$\frac{10^m}{1^h 27} = \frac{600}{200} = 3.69 = 207$$

$$\begin{array}{r} 26' 50'' \\ 60'' \\ \hline \end{array}$$

$$33' 10'' = 1990 : 200 = 1$$

$$\begin{array}{r} 44' 20'' \\ 100'' \\ \hline \end{array}$$

$$352' \quad 1390 : \quad 165 :$$

$$45' 20''$$

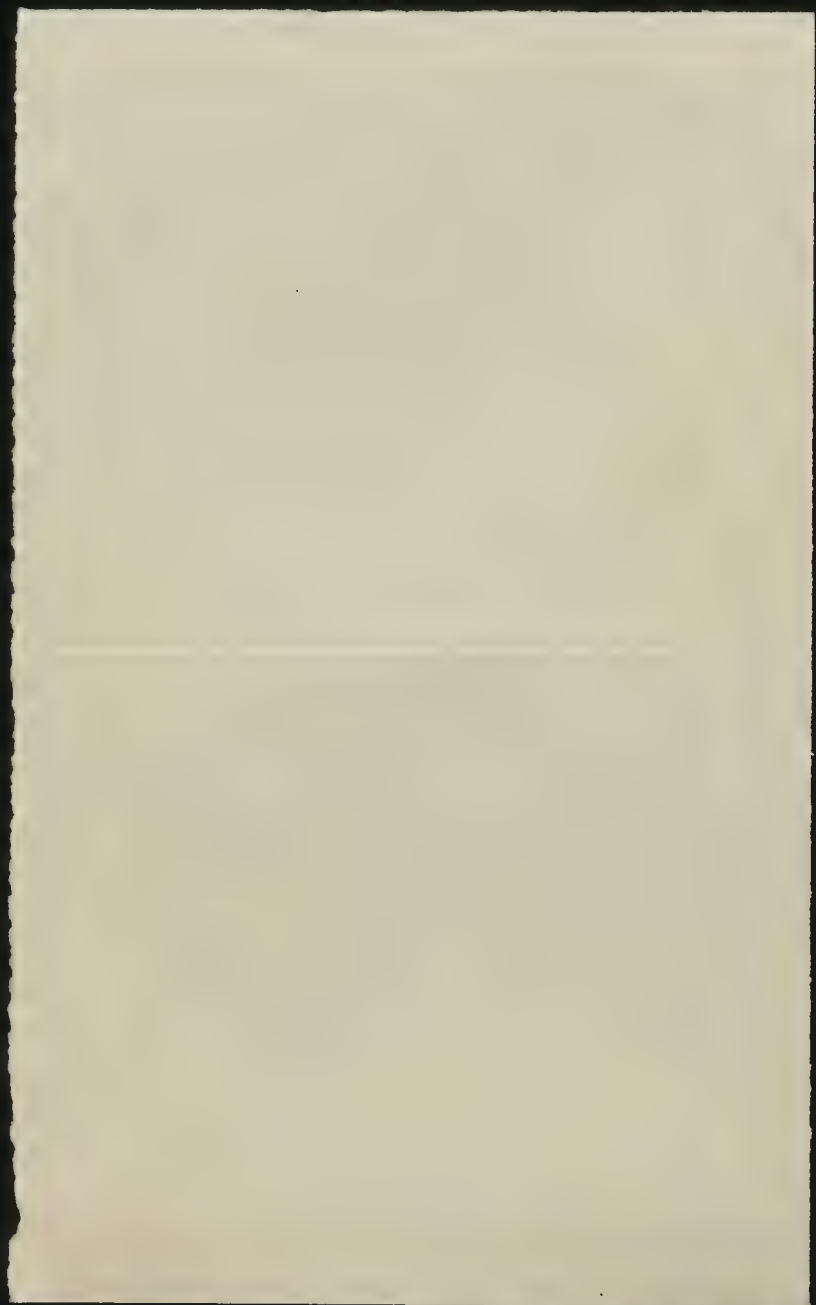
$$5' 20''$$

$$239''$$

$$\begin{array}{r} 200 \\ \hline 42 \\ \hline 158 \end{array} \quad \begin{array}{r} 0.7 \\ 215.14 \\ \hline 115 \\ \hline 55 \end{array}$$

$$19000 : 198 \quad 295000$$





čas do repetitív

$$\begin{array}{rcl} R : 1 \text{ eta} & 3 \text{ m } 35 & = 215 \\ & 2 & 27 = 147 \\ & 2'7-3'5 & 1 \cdot 55 = 115 \end{array}$$

$$\begin{array}{r} 215 : 147 = 146 \neq \sqrt{2} \\ 68 \\ 9 \end{array}$$

$$\begin{array}{r} 215 : 115 = 179 \neq \sqrt{3} \\ 100 \\ 19 \end{array}$$

rozrysanie nastupaji poz 2'4 eta.

(stannut)

water van de

-1

2 min 2 sec / 1-57

1 45 / 1.45

16

21

25

Van 60

3 min 55

2 min 45 sec

Nie  
uszel  
!



48.

82

74.2

44.2

50 = 33

34.7

60 = 42.5

24.7

~~70~~

52.5

12.2

26

62

Nie r

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